

Fizika 2

(PREDAVANJA)

UVOD

SILE

Kvalitativno: fizikalne količine, ki podajajo vpliv okolice na opazovano telo oz. sistem

Kvantitativno: temelj na 5 pravilih (definicije, predpostavke / fizikalni zakoni /)

\vec{F} ... skupna sila okolice na opazovano telo

m ... masa opazovanega telesa

\vec{v} ... hitrost opazovanega telesa

\vec{a} ... pospešek opazovanega telesa

d_{\min} ... minimalna razdalja opazovanega telesa od okoljskih teles

(1) (predpostavka): $\lim_{d_{\min} \rightarrow \infty} \vec{F} = \vec{0}$

(2) (definicija inercialnega opazovalnega / koordinatnega / sistema)

$$d_{\min} \rightarrow \infty \stackrel{!}{\Rightarrow} \vec{F} = \vec{0}: \quad \text{S: } \vec{v} = \text{konst.} \stackrel{(\text{def.})}{\Rightarrow} \text{S inercialen}$$

\uparrow
sistem

Komentar: 1. Newtonov zakon v smislu zgornje definicije.

(3) (definicija \vec{F}): S inercialen, \vec{a}, m

$$\vec{F} \equiv m \cdot \vec{a}$$

Komentar: 2. Newtonov zakon; $\vec{a} = 0 \Rightarrow \vec{F} = 0$

(1. Newtonov zakon)

Komentar: daljnosežne implikacije

(4) (zabon - načelo superpozicije)

\vec{F}_i ... sila i -tega okoljskega telesa na opazovano telo

(če so vsa ostala okoljska telesa daleč stran $\Rightarrow \vec{F} = \vec{F}_i$)

$$\vec{F} = \sum_i \vec{F}_i$$

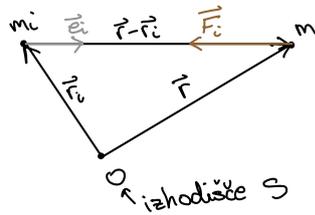
Komentar: Newton v 'Principih' (Axioms or laws of motion), Besledica 1
-ta zakon samo posledica prvih dveh zakonov

(5) (definicija): dve telesi: $\vec{F}_{1 \rightarrow 2}$ in $\vec{F}_{2 \rightarrow 1}$

Če velja: $\vec{F}_{2 \rightarrow 1} = -\vec{F}_{1 \rightarrow 2}$, potem za sili $\vec{F}_{1 \rightarrow 2}$ in $\vec{F}_{2 \rightarrow 1}$ velja 3. Newtonov zakon.

(def.)

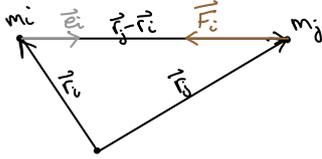
PRIMER:



$$\hat{e}_i = \frac{(\vec{r} - \vec{r}_i)}{|\vec{r} - \vec{r}_i|}$$

$$\vec{F}_i = -\frac{k m_i m}{|\vec{r} - \vec{r}_i|^2} \hat{e}_i = -\frac{k m_i m}{|\vec{r} - \vec{r}_i|^3} (\vec{r} - \vec{r}_i)$$

$$|\vec{r} - \vec{r}_i| \rightarrow \infty : \lim_{|\vec{r} - \vec{r}_i| \rightarrow \infty} \vec{F}_i = 0$$



$$\vec{F}_{i \rightarrow j} = -\frac{k m_i m_j}{|\vec{r}_j - \vec{r}_i|^3} (\vec{r}_j - \vec{r}_i) \quad |\vec{r}_i - \vec{r}_j|^3 = |\vec{r}_j - \vec{r}_i|^3 \wedge (\vec{r}_i - \vec{r}_j) = -(\vec{r}_j - \vec{r}_i)$$

$$\vec{F}_{j \rightarrow i} = -\frac{k m_i m_j}{|\vec{r}_i - \vec{r}_j|^3} (\vec{r}_i - \vec{r}_j) = \frac{k m_i m_j}{|\vec{r}_j - \vec{r}_i|^3} (\vec{r}_j - \vec{r}_i) = -\vec{F}_{i \rightarrow j}$$

(velja 3. Newtonov zakon)

GIBALNA KOLIČINA

\vec{F}_n ... skupna sila na l. telo

m_n ... masa l. telesa

\vec{v}_n ... hitrost l. telesa

$\int_{t_1}^{t_2} \vec{F}_n dt$... surnek vseh sil na l. telo (t_1, t_2 začetni in končni čas)

$G_n = m_n \cdot \vec{v}_n$... gibalna količina l. telesa

$$\Delta \vec{G}_n = \vec{G}_{n,k} - \vec{G}_{n,l}$$

IZREK: $\int_{t_1}^{t_2} \vec{F}_i dt = \Delta \vec{G}_i$

$$\Delta \vec{G}_i = \vec{G}_{i,2} - \vec{G}_{i,1} ; \quad \vec{G}_{i,1} = m_i \cdot \vec{v}_{i,1} \quad m_i = \text{konst.} / m \neq m(v)$$

$$\vec{G}_{i,2} = m_i \cdot \vec{v}_{i,2}$$

Dokaz: $\int_{t_1}^{t_2} \vec{F}_i dt \stackrel{(3)}{=} \int_{t_1}^{t_2} m_i \vec{a}_i dt = \int_{t_1}^{t_2} m_i \dot{\vec{v}}_i dt = \int_{t_1}^{t_2} (m_i \dot{\vec{v}}_i) dt = m_i \vec{v}_i \Big|_{t_1}^{t_2} = m_i \vec{v}_{i,2} - m_i \vec{v}_{i,1} = \Delta \vec{G}_i \quad \square$

SISTEM 2 TELES:

$$\vec{G} = \vec{G}_1 + \vec{G}_2 ; \quad \vec{G}_2 = \vec{G}_{1,2} + \vec{G}_{2,2}$$

$$\vec{G}_k = \vec{G}_{1,k} + \vec{G}_{2,k}$$

$\vec{F}_{2 \rightarrow 1}, \vec{F}_{1 \rightarrow 2}$... "notranji" sili
 \vec{F}_1, \vec{F}_2 ... skupni sili
 $\vec{F}_{1,2} = \vec{F}_1 - \vec{F}_{2 \rightarrow 1}$
 $\vec{F}_{2,1} = \vec{F}_2 - \vec{F}_{1 \rightarrow 2}$ } "zunanji" sili

$$\int_{t_a}^{t_b} \vec{F}_1 dt = \vec{G}_{1,1k} - \vec{G}_{1,1z}$$

$$\int_{t_a}^{t_b} (\vec{F}_{1,2} + \vec{F}_{2,1}) dt = \int_{t_a}^{t_b} \vec{F}_{1,2} dt + \int_{t_a}^{t_b} \vec{F}_{2,1} dt = \vec{G}_{1,1k} + \vec{G}_{1,1z}$$

$$\int_{t_a}^{t_b} \vec{F}_{1,2} dt + \int_{t_a}^{t_b} \vec{F}_{1,2} dt = \vec{G}_{2,1k} - \vec{G}_{2,1z}$$

Predpostavka: $\vec{F}_{2,1} = -\vec{F}_{1,2}$ ← velja 3. Newtonov zakon

$$\int_{t_a}^{t_b} \vec{F}_{1,2} dt + \int_{t_a}^{t_b} \vec{F}_{2,2} dt + \int_{t_a}^{t_b} \vec{F}_{2,1} dt + \int_{t_a}^{t_b} \vec{F}_{1,2} dt =$$

$$= \int_{t_a}^{t_b} (\vec{F}_{1,2} + \vec{F}_{2,2}) dt + \int_{t_a}^{t_b} (\vec{F}_{2,1} + \vec{F}_{1,2}) dt = \int_{t_a}^{t_b} \vec{F}_z dt ; \vec{F}_z = \vec{F}_{1,2} + \vec{F}_{2,2}$$

$$\vec{G}_{1,1k} + \vec{G}_{2,1k} - \vec{G}_{1,1z} - \vec{G}_{2,1z} = \vec{G}_k - \vec{G}_z = \Delta \vec{G} \quad (\text{razlika skupne gibalne količine})$$

$$\Rightarrow \int_{t_a}^{t_b} \vec{F}_z dt = \Delta \vec{G}$$

Primer:

$$\int_{t_a}^{t_b} \vec{F}_z dt = 0 \quad \leftarrow \text{sistem izoliran od okolice}$$

$$\Rightarrow \Delta \vec{G} = 0 \quad \text{ali} \quad \vec{G}_k = \vec{G}_z \quad \leftarrow \text{gibalna količina se ohranja}$$

GALILEJEVE TRANSFORMACIJE (*)

sistem S, izhodišče O } \vec{r}_0
sistem S', izhodišče O' }

$$\vec{r}_0 = \vec{v}_0 t ; \vec{v}_0 = \text{konst.}$$

$$\vec{r} = \vec{r}_0 + \vec{r}'$$

$$\Rightarrow \vec{r}' = \vec{r} - \vec{r}_0 = \vec{r} - \vec{v}_0 t$$

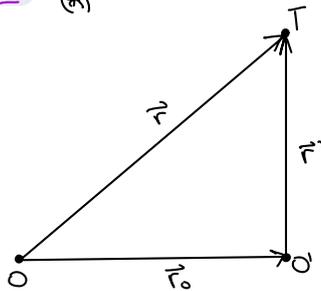
$$\vec{v} \equiv \frac{d\vec{r}}{dt}$$

Predpostavka: $t = t'$

$$\vec{v}' \equiv \frac{d\vec{r}'}{dt'} = \frac{d\vec{r}'}{dt} = \frac{d}{dt}(\vec{r} - \vec{v}_0 t) = \frac{d\vec{r}}{dt} - \frac{d}{dt}(\vec{v}_0 t) = \vec{v} - \vec{v}_0$$

$$\vec{a} \equiv \frac{d\vec{v}}{dt}$$

$$\vec{a}' \equiv \frac{d\vec{v}'}{dt'} = \frac{d\vec{v}'}{dt} = \frac{d}{dt}(\vec{v} - \vec{v}_0) = \frac{d\vec{v}}{dt} = \vec{a}$$



(1) S inercialen sistem \Rightarrow S' inercialen sistem

$$\vec{F} = 0 \Rightarrow \vec{a} = 0 \Rightarrow \vec{a}' = 0$$

(2) \vec{F}' skupna sila na telo v S': $\vec{F}' = m' \cdot \vec{a}'$; $m' = m$ (predpostavka)
 $= m \cdot \vec{a}$ $\vec{a}' = \vec{a}$ (*)
 $= \vec{F}$ ← sile invariante

MATRIČNI ZAPIS GALILEJEVIH TRANSFORMACIJ:

$$\hat{e}_x = \hat{e}'_x; \quad \hat{e}_y = \hat{e}'_y; \quad \hat{e}_z = \hat{e}'_z$$

$$\vec{v}_0 = v_0 \cdot \hat{e}_x$$

$$\vec{r} = x \hat{e}_x + y \hat{e}_y + z \hat{e}_z = \begin{bmatrix} x \\ y \\ z \end{bmatrix}$$

$$\begin{aligned} \vec{r}' &= x' \hat{e}'_x + y' \hat{e}'_y + z' \hat{e}'_z = \begin{bmatrix} x' \\ y' \\ z' \end{bmatrix} \\ &= x \hat{e}_x + y \hat{e}_y + z \hat{e}_z = \begin{bmatrix} x \\ y \\ z \end{bmatrix} \end{aligned}$$

$$\vec{r}' = \vec{r} - \vec{v}_0 t = \begin{bmatrix} x - v_0 t \\ y \\ z \end{bmatrix}$$

$$\overset{\substack{\uparrow \\ \text{4-dimenzije}}}{(4)} X = \begin{bmatrix} c_0 t \\ x \\ y \\ z \end{bmatrix} \Rightarrow (4) X = \begin{bmatrix} c_0 t' \\ x' \\ y' \\ z' \end{bmatrix} = \begin{bmatrix} c_0 t \\ x - v_0 t \\ y \\ z \end{bmatrix}$$

c_0 - hitrost svetlobe v vakuumu

$$(a \neq \vec{a}) \quad G = \begin{bmatrix} 1 & 0 & 0 & 0 \\ -\beta_0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}; \quad \beta_0 = \frac{v_0}{c_0}$$

← matrika Galilejeve transformacije

$$\Rightarrow (4) X' = G (4) X$$

$$S_0 \rightarrow S_1: v_1, \beta_1 = \frac{v_1}{c_0} : G_1 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ -\beta_1 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

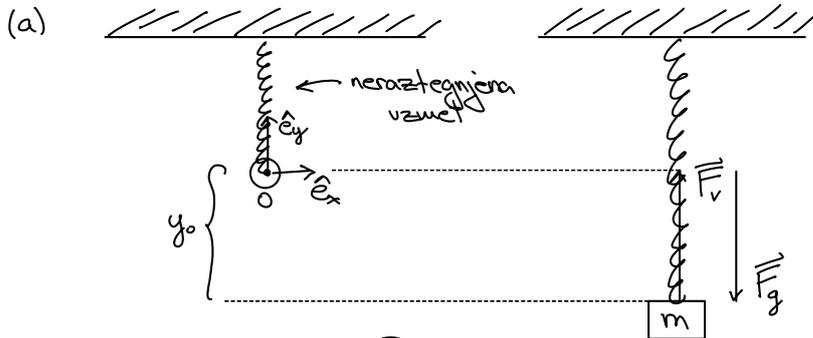
$$S_1 \rightarrow S_2: v_2; \beta_2 = \frac{v_2}{c_0} : G_2 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ -\beta_2 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$S_0 \rightarrow S_1 \rightarrow S_2: G_2 G_1 = \begin{bmatrix} 1 & 0 & 0 & 0 \\ -\beta_2 \beta_1 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \Leftarrow S_0 \rightarrow S_2$$

1. MEHANSKO NIHANJE in VALOVANJE

ENOSTAINA NIHALA - ENAČBA (LASTNEGA DUŠENEGA) NIHANJA

UTEŽ NA VISAČNI VZMETI



$$\vec{F}_g = \begin{bmatrix} 0 \\ -mg_0 \\ 0 \end{bmatrix} \quad \vec{F}_v = \begin{bmatrix} 0 \\ -ky_0 \\ 0 \end{bmatrix} \quad ; \quad \left. \begin{array}{l} y_0 < 0 \\ k > 0 \end{array} \right\} \Rightarrow -ky_0 > 0 \Rightarrow \vec{F}_v \uparrow$$

$g_0 \sim 10 \frac{m}{s^2}$ (Hookov zakon)

$$\Rightarrow \boxed{mg_0 = -ky_0}$$

Tudi (3) in (4): (3) $\vec{a} = 0 \Rightarrow \vec{F} = 0$

$$(4): \vec{F} = \vec{F}_g + \vec{F}_v = -mg_0 \hat{e}_y - ky_0 \hat{e}_y = -(mg_0 + ky_0) \hat{e}_y = 0$$

(b) v smeri \hat{e}_y : $y_0 \rightarrow y$
 po (3): $\vec{F} = m \cdot \vec{a} = m \cdot \vec{v} = m \cdot \dot{\vec{r}}$; $\vec{r} = \begin{bmatrix} x \\ y \\ z \end{bmatrix} \Rightarrow \dot{\vec{r}} = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{bmatrix} = \dot{x} \hat{e}_x + \dot{y} \hat{e}_y + \dot{z} \hat{e}_z$

po (4): $\vec{F} = \vec{F}_g + \vec{F}_v + \vec{F}_u$ (sila upora)

$$\vec{F}_g = -mg_0 \hat{e}_y; \quad \vec{F}_v = -ky_0 \hat{e}_y; \quad \vec{F}_u = -C\dot{y}; \quad C > 0 \rightarrow \vec{v} = -C\dot{y} \hat{e}_y = -C\dot{y} \hat{e}_y$$

LINEARNI ZAKON UPORA

$$(-mg_0 - ky_0 - C\dot{y}) \hat{e}_y = m\ddot{x} \hat{e}_x + m\ddot{y} \hat{e}_y + m\ddot{z} \hat{e}_z$$

$$\Rightarrow m\ddot{x} \hat{e}_x + (mg_0 + ky_0 + C\dot{y} + m\ddot{y}) \hat{e}_y + m\ddot{z} \hat{e}_z = 0$$

$$\Rightarrow \begin{cases} m\ddot{x} = 0 \\ m\ddot{y} + mg_0 + ky_0 + C\dot{y} = 0 \\ m\ddot{z} = 0 \end{cases}$$

$$\Rightarrow \dot{x} = \text{konst.}$$

$$v_x(t=0) = 0 \Rightarrow \dot{x} = 0 \Rightarrow x = \text{konst.}$$

$$\Rightarrow z = \text{konst.}$$

$$\Rightarrow \underline{z = 0}$$

$$\Rightarrow \underline{z = 0}$$

$$m\ddot{y} + C\dot{y} + ky_0 - \overbrace{ky_0}^{mg_0} = 0 \quad /: m$$

$$\Rightarrow \ddot{y} + \beta \dot{y} + \omega_0^2 (y - y_0) = 0; \quad \beta = \frac{C}{m} > 0 \quad [\beta] = s^{-1}$$

$$\omega_0^2 = \frac{k}{m} \quad \leftarrow \text{KOEFIČIENT DUŠENJA} \quad [\omega_0^2] = s^{-2}$$

$$\begin{aligned} y' &= y - y_0 \\ y'' &= \dot{y}, \quad \dot{y}' = \ddot{y} \\ &\Rightarrow y = y' + y_0 \end{aligned}$$

$$\Rightarrow \boxed{\ddot{y}' + \beta \dot{y}' + \omega_0^2 y' = 0} \quad \leftarrow \text{ENAČBA (DUŠENEGA LASTNEGA) NIHANJA}$$

(homogena linearna diferencialna enačba 2. reda s konstantnimi koeficienti)

Reševanje enačbe $\ddot{y}' + \beta \dot{y}' + \omega_0^2 y' = 0$:

$$y' = Ae^{\lambda t}; \quad A, \lambda \text{ konst.}$$

$$\Rightarrow \dot{y}' = \lambda y' \quad \text{in} \quad \ddot{y}' = \lambda^2 y'$$

$$\Rightarrow (\lambda^2 + \beta \lambda + \omega_0^2) Ae^{\lambda t} = 0 \quad \text{za} \quad \forall t$$

$$(1) A = 0 \Rightarrow y' = 0 \quad \leftarrow \text{TRIVIALNA REŠITEV}$$

(2) Rešujemo torej kvadratno enačbo: $\lambda^2 + \beta \lambda + \omega_0^2 = 0$.

$$D = \beta^2 - 4\omega_0^2 \equiv -4\omega^2$$

$$\Rightarrow \omega^2 = \omega_0^2 - \frac{\beta^2}{4}$$

Dobimo več možnosti:

(a) $D < 0$ ($\omega^2 > 0$): **PODKRITIČNO DUŠENJE**

$$\sqrt{D} = \sqrt{-4\omega^2} = 2i\omega; \quad \omega = +\sqrt{\omega^2}$$

$$\lambda_{1,2} = \frac{-\beta \pm 2i\omega}{2} = -\frac{\beta}{2} \pm i\omega$$

$$\Rightarrow \underset{\text{in}}{y'_1} = A_1 \exp\left(-\frac{\beta}{2}t + i\omega t\right) = A_1 \exp\left(-\frac{\beta}{2}t\right) \exp(i\omega t)$$

$$y'_2 = A_2 \exp\left(-\frac{\beta}{2}t\right) \exp(-i\omega t)$$

$$\ddot{y}'_1 + \beta \dot{y}'_1 + \omega_0^2 y'_1 = 0 \quad \text{in} \quad \ddot{y}'_2 + \beta \dot{y}'_2 + \omega_0^2 y'_2 = 0$$

Enačba linearna $\Rightarrow y' = y'_1 + y'_2$ tudi rešitev

$$(y'_1 + y'_2)'' + \beta(y'_1 + y'_2)' + \omega_0^2(y'_1 + y'_2) = \ddot{y}'_1 + \ddot{y}'_2 + \beta \dot{y}'_1 + \beta \dot{y}'_2 + \omega_0^2 y'_1 + \omega_0^2 y'_2 = 0$$

$$\Rightarrow y' = \exp\left(-\frac{\beta}{2}t\right) [A_1 \exp(i\omega t) + A_2 \exp(-i\omega t)]$$

Uporabimo Eulerjevo formulo: $\exp(\pm i\omega t) = \cos(\omega t) \pm i \sin(\omega t)$

$$\Rightarrow y' = \exp\left(-\frac{\beta}{2}t\right) [(A_1 + A_2) \cos(\omega t) + i(A_1 - A_2) \sin(\omega t)] =$$

$$= \exp\left(-\frac{\beta}{2}t\right) [B_1 \cos(\omega t) + B_2 \sin(\omega t)]$$

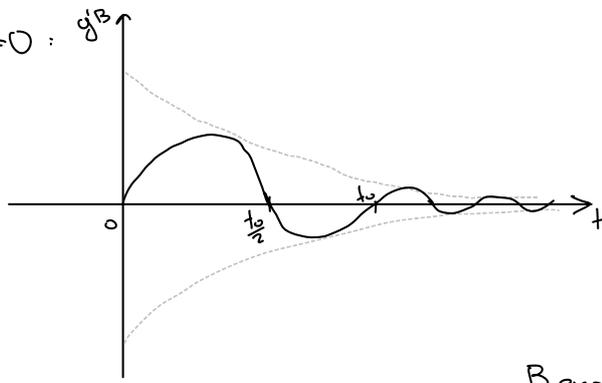
$$= \boxed{B \exp\left(-\frac{\beta}{2}t\right) \sin(\omega t + \delta)} \quad \leftarrow \text{"fazni premik"}$$

$$\sin(\omega t + \delta) = \cos \delta \sin(\omega t) + \sin \delta \cos(\omega t)$$

$$\Rightarrow B \exp\left(-\frac{\beta}{2}t\right) \sin(\omega t + \delta) = \exp\left(-\frac{\beta}{2}t\right) [B \cos \delta \sin(\omega t) + B \sin \delta \cos(\omega t)]$$

$$\Rightarrow B_1 = B \sin \delta, \quad B_2 = B \cos \delta, \quad \tan \delta = \frac{B_1}{B_2} \quad \rightarrow \quad B = +\sqrt{B_1^2 + B_2^2}$$

Primer: $\delta = 0$: y^B



t_0 = lastni nihajni čas

$$\omega t_0 = 2\pi \Rightarrow t_0 = \frac{2\pi}{\omega}$$

$$\gamma = \frac{1}{t_0} \Rightarrow \omega = 2\pi\gamma$$

$$B \exp\left(-\frac{\beta}{2}t\right) \leftarrow \text{DUŠENJE}$$

B in δ iz "začetnih" pogojev:

$$y'(t=0) \text{ in } \dot{y}(t=0)$$

$$y(t) = B \exp\left(-\frac{\beta}{2}t\right) \sin(\omega t + \delta) \Rightarrow y'(t=0) = B \sin \delta$$

$$\dot{y}(t) = -\frac{\beta}{2} B \exp\left(-\frac{\beta}{2}t\right) \sin(\omega t + \delta) + B \omega \exp\left(-\frac{\beta}{2}t\right) \cos(\omega t + \delta)$$

$$\Rightarrow \dot{y}(t=0) = -\frac{\beta}{2} B \sin \delta + B \omega \cos \delta$$

ENERGIJA NIHALA

$$W_k = \frac{1}{2} m v^2 = \frac{1}{2} m (\dot{y})^2 \rightarrow v = \dot{y} = \dot{y} \quad (y \neq \dot{y})$$

$$W_{pr} = \frac{1}{2} k y^2 = \frac{1}{2} k (y' + y_0)^2$$

$$W_p = m g_0 y = m g_0 (y' + y_0)$$

$$\Rightarrow W = W_k + W_p + W_{pr}$$

Primer: nedušeno nihanje: $\beta \rightarrow 0$

$$\omega^2 = \omega_0^2 - \frac{\beta^2}{4} = \omega_0^2 = \frac{k}{m}$$

$$\Rightarrow y' = B \exp\left(-\frac{\beta}{2}t\right) \sin(\omega t + \delta) = B \sin(\omega t + \delta)$$

$$\Rightarrow \dot{y}' = B \omega_0 \cos(\omega t + \delta)$$

$$W_k = \frac{1}{2} m B^2 \omega_0^2 \cos^2(\omega t + \delta) = \frac{1}{2} m B^2 \frac{k}{m} \cos^2(\omega t + \delta) = \frac{k B^2}{2} \cos^2(\omega t + \delta)$$

$$W_{pr} = \frac{1}{2} k B^2 \sin^2(\omega t + \delta) + k y_0 B \sin(\omega t + \delta) + \frac{1}{2} k y_0^2$$

$$W_p = m g_0 y_0 + m g_0 B \sin(\omega t + \delta)$$

$$\Rightarrow W = \frac{1}{2} k B^2 + \underbrace{(k y_0 + m g_0)}_{=0} B \sin(\omega t + \delta) + \frac{1}{2} k y_0^2 + m g_0 y_0$$

$$\Rightarrow W = \frac{1}{2} k B^2 + \frac{1}{2} k y_0^2 + m g_0 y_0 = \frac{1}{2} k B^2 - \frac{1}{2} k y_0^2 = \text{konst.}$$

Dušenje: $B \rightarrow B \exp\left(-\frac{\beta}{2}t\right)$

(b) $D=0$ ($\omega=0$): KRITIČNO DUŠENJE

$$\lambda = -\frac{\beta}{2} \Rightarrow y_1 = B_1 \exp\left(-\frac{\beta}{2}t\right)$$

Trdimo: $y_2 = B_2 t \exp\left(-\frac{\beta}{2}t\right)$ tudi rešitev

$$\Rightarrow y' = (B_1 + B_2 t) \exp(-\frac{\beta}{2} t)$$

(c) $D > 0$ ($\omega^2 < 0$): **NADKRITIČNO DUŠENJE**

$$D = -4\omega^2 > 0 \Rightarrow \omega^2 < 0 \Rightarrow \omega = \pm i|\omega|$$

$$D = 4|\omega|^2 \Rightarrow \lambda_{1,2} = -\frac{\beta}{2} \pm |\omega|$$

$$\Rightarrow y' = B_1 \exp(\lambda_1 t) + B_2 \exp(\lambda_2 t); \quad \lambda_2 = -\frac{\beta}{2} - |\omega| < 0 \quad \checkmark$$

$$\lambda_1 = -\frac{\beta}{2} + |\omega| < 0 \quad \checkmark$$

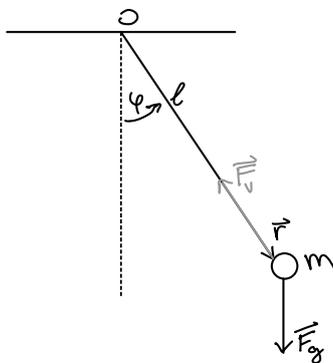
$$\omega^2 = \omega_0^2 - \frac{\beta^2}{4} < 0 \rightarrow -\omega^2 = \frac{\beta^2}{4} - \omega_0^2 = |\omega|^2 \rightarrow |\omega| = \frac{\beta}{2} \sqrt{1 - \frac{4\omega_0^2}{\beta^2}} < \frac{\beta}{2}$$

Zelo močno dušenje:

$$\frac{4\omega_0^2}{\beta^2} \ll 1 \Rightarrow |\omega| = \frac{\beta}{2} (1 - \frac{2\omega_0^2}{\beta^2})$$

$$\lambda_1 = \frac{-\frac{\beta}{2} + \frac{\beta}{2} - \frac{\omega_0^2}{\frac{\beta^2}{4}}}{0} \approx -\frac{4\omega_0^2}{\beta}$$

NITNO ali **MATEMATIČNO NIHALO** (nedušeno)



$$\vec{M} = \vec{r} \times \vec{F}_g + \vec{r} \times \vec{F}_v = \vec{r} \times \vec{F}_g$$

$\vec{0} \leftarrow \vec{r} \parallel \vec{F}_v$

$$\vec{F}_g = -m g_0 \hat{e}_y; \quad \vec{r} = l \sin \varphi \hat{e}_x - l \cos \varphi \hat{e}_y$$

$$\vec{M} = \vec{r} \times \vec{F}_g = -m g_0 l \sin \varphi \hat{e}_x \times \hat{e}_y = -m g_0 l \sin \varphi \hat{e}_z$$

$$\Rightarrow \vec{M} = M_z \hat{e}_z \Rightarrow \boxed{M_z = -m g_0 l \sin \varphi}$$

Newtonov zakon za vrtenje okoli fiksne osi: (\hat{e}_z)

$$\boxed{M_z = I_z \alpha = I_z \ddot{\varphi}}; \quad I_z = m l^2$$

$$-m g_0 l \sin \varphi = m l^2 \ddot{\varphi} \Rightarrow \boxed{\ddot{\varphi} + \frac{g_0}{l} \sin \varphi = 0}$$

$$\varphi \ll 1 \quad ([\varphi] = \text{rad}) \Rightarrow \text{Taylor: } \sin \varphi \sim \varphi$$

$$\Rightarrow \boxed{\ddot{\varphi} + \frac{g_0}{l} \varphi = 0} \quad \omega_0^2 = \frac{g_0}{l} \Rightarrow \boxed{t_0 = \frac{2\pi}{\omega_0} = 2\pi \sqrt{\frac{l}{g_0}}}$$

← enačba nihanja

1. POSKUS: t_0 nitnega nihala

$$t_{10} \rightarrow t_0 = \frac{t_{10}}{10}$$

$$t_{10} = 19,87 \text{ s} \Rightarrow t_0 = 1,99 \text{ s}$$

$$t_0 = 2\pi \sqrt{\frac{l}{g_0}} \xrightarrow{10 \frac{\text{m}}{\text{s}^2}} l = 1 \text{ m} \Rightarrow t_0 = 2\pi \sqrt{\frac{1}{10}} \text{ s} = 2\pi \cdot 0,316 \text{ s} = 2 \text{ s}$$

↗ majhno odstopanje

2. POSKUS: to nihala na vijačno vzmet:

$$t_{10} = 13'24 \text{ s} \Rightarrow \underline{t_0 \approx 1'3 \text{ s}}$$

$$t_0 = 2\pi \sqrt{\frac{m}{k}}; \quad m = 400 \text{ g} = 0'4 \text{ kg}$$

$$\underline{t_0} = 2\pi \sqrt{\frac{2m_1 \cdot x}{m_1 g_0}} = 2\pi \sqrt{\frac{2 \cdot 0'2 \text{ m}}{10 \text{ m/s}^2}} =$$

$$\underline{= 1'2 \text{ s}}$$

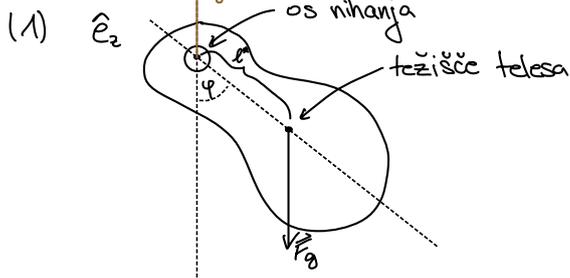
$$F_v = kx$$

$$F_g = m \cdot g_0$$

$$x = 0'2 \text{ m}$$

$$\Delta m = 0'2 \text{ kg} \Rightarrow k = \frac{m \cdot g_0}{x}$$

FIZIČNA NIHALA



M_z : navor vseh sil okoli osi

$$\vec{M}_0 = \vec{r}_0 \times \vec{F}_0 = \vec{0} \quad (\vec{r}_0 = 0)$$

$$M_z = -mg l^* \sin \varphi \quad (M_g \dots \text{navor sile teže})$$

$$M_z = J_z \alpha$$

vztrajnostni moment (odvisnost m, oblike)

$$\alpha = \ddot{\varphi}$$

$$\Rightarrow -mg l^* \sin \varphi = J_z \ddot{\varphi} \Rightarrow \ddot{\varphi} + \frac{mg l^*}{J_z} \sin \varphi = 0$$

$$\varphi \ll 1: \sin \varphi \approx \varphi \Rightarrow \ddot{\varphi} + \frac{mg_0 l^*}{J_z} \varphi = 0$$

$$\omega_0^2 = \frac{mg_0 l^*}{J_z}$$

$$t_0 = \frac{2\pi}{\omega_0}$$

Primer: $l^* = \frac{l}{2}$

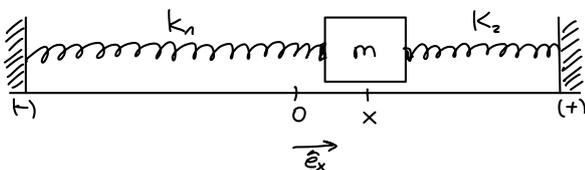
$$J_z = \frac{1}{12} ml^2 + m \left(\frac{l}{2}\right)^2 = \left(\frac{1}{12} + \frac{1}{4}\right) ml^2 = \frac{1}{3} ml^2$$

(vrtenje okrog osi) (premik)

$$\Rightarrow \omega_0^2 = \frac{3mg_0 l}{2 ml^2} = \frac{3}{2} \frac{g_0}{l}$$

$$\Rightarrow t_0 = \frac{2\pi}{\omega_0} = 2\pi \sqrt{\frac{2}{3} \frac{l}{g_0}}$$

(2)



$$\left. \begin{array}{l} \text{a) } l_{1,10} \\ \text{b) } l_{1,1r} \end{array} \right\} \Rightarrow \Delta l_{1,r} = l_{1,r} - l_{1,10} \Rightarrow \vec{F}_{1,r} = -k_1 \Delta l_{1,r} \hat{e}_x$$

$$\text{sila druge vzmeti } \vec{F}_{2,r} = k_2 \Delta l_{2,r} \hat{e}_x$$

sila prve vzmeti

$$\vec{F}_1 + \vec{F}_2 + \underbrace{\vec{F}_g + \vec{F}_r}_{=\vec{0}} = \vec{F}_1 + \vec{F}_2$$

V ravnovesni legi: $\vec{F}_1 = \vec{F}_{1,r}$, $\vec{F}_2 = \vec{F}_{2,r}$

$$\Rightarrow \vec{F}_{1,r} + \vec{F}_{2,r} = \vec{0} \Rightarrow (-k_1 \Delta l_{1,r} + k_2 \Delta l_{2,r}) \hat{e}_x = 0$$

$$\Rightarrow \boxed{\frac{\Delta l_{1,r}}{\Delta l_{2,r}} = \frac{k_2}{k_1}}$$

c) telo v legi x:

$$\Delta l_1 = \Delta l_{1,r} + x \quad \text{in} \quad \Delta l_2 = \Delta l_{2,r} - x$$

$$\Rightarrow \vec{F}_1 = -k_1 \Delta l_1 \hat{e}_x = -k_1 \Delta l_{1,r} \hat{e}_x - k_1 x \hat{e}_x = \vec{F}_{1,r} - k_1 x \hat{e}_x$$

$$\Rightarrow \vec{F}_2 = k_2 \Delta l_2 \hat{e}_x = k_2 \Delta l_{2,r} \hat{e}_x - k_2 x \hat{e}_x = \vec{F}_{2,r} - k_2 x \hat{e}_x$$

$$\Rightarrow \vec{F}_1 + \vec{F}_2 = \vec{F}_{1,r} - k_1 x \hat{e}_x + \vec{F}_{2,r} - k_2 x \hat{e}_x \stackrel{(*)}{=} \boxed{-(k_1 + k_2)x \hat{e}_x = m \ddot{x} \hat{e}_x}$$

$$\Rightarrow (m \ddot{x} + (k_1 + k_2)x) \hat{e}_x = 0$$

$$\Rightarrow \boxed{\ddot{x} + \frac{k_1 + k_2}{m} x = 0} \leftarrow \text{ENAČBA NIHANJA}$$

$$\Rightarrow \omega_0^2 = \frac{k_1 + k_2}{m}$$

$$\Rightarrow \boxed{T_0 = \frac{2\pi}{\omega_0} = 2\pi \sqrt{\frac{m}{k_1 + k_2}}}$$

VSILJENO (DUŠENO) NIHANJE

Spomnimo se: $[m\ddot{y} + \underbrace{C\dot{y} + k(y-y_0)}_{\Sigma F}] \hat{e}_y = 0$

$$y' = y - y_0$$

$$\Rightarrow \boxed{m\ddot{y}' + C\dot{y}' + ky' = 0}$$

Dodatna (vsiljena) sila: sinusna: $\lambda_v = \omega_v = 2\pi \nu_v$

$$\Sigma \vec{F} = -(C\dot{y}' + k(y-y_0)) \hat{e}_y + \vec{F}_v; \quad \vec{F}_v = F_0 \sin(\omega_v t) \hat{e}_y$$

↑
amplituda vsiljenja

$$\boxed{m\ddot{y}' + C\dot{y}' + ky' = F_0 \sin(\omega_v t)} \leftarrow \text{ENAČBA VSILJENEGA NIHANJA}$$

(nehomogena)

$$\boxed{\ddot{y}' + \beta \dot{y}' + \omega_0^2 y' = \frac{F_0}{m} \sin(\omega_v t)}$$

← rešitev homogenega dela
 $y' = y'_h + y'_p$ ← partikularna rešitev

$$y'_h = B e^{(-\frac{C}{2m}t)} \sin(\omega t + \delta) \quad (\text{podkritično nihanje})$$

$$\frac{C}{2m} \gg 1 \Rightarrow y'_h \rightarrow 0$$

$$y'_p = B_p \sin(\omega_v t - \delta_p) \leftarrow \text{nastavek}$$

$$(y''_h + y''_p) + \beta(y'_h + y'_p) + \omega_0^2(y_h + y_p) = \frac{F_0}{m} \sin(\omega_v t)$$

$$\underbrace{\ddot{y}_h + \beta \dot{y}_h + \omega_0^2 y_h}_{=0} + \ddot{y}_p + \beta \dot{y}_p + \omega_0^2 y_p = \frac{F_0}{m} \sin(\omega_v t)$$

$$\text{Rešujemo enačbo: } \ddot{y}_p + \beta \dot{y}_p + \omega_0^2 y_p = \frac{F_0}{m} \sin(\omega_v t)$$

$$y_p = B_p [\sin(\omega_v t) \cos \delta_p - \sin \delta_p \cos(\omega_v t)] \leftarrow \text{NASTAVEK}$$

$$\dot{y}_p = \omega_v B_p \cos(\omega_v t - \delta_p) = \omega_v B_p [\cos(\omega_v t) \cos \delta_p + \sin(\omega_v t) \sin \delta_p]$$

$$\ddot{y}_p = \omega_v^2 B_p \sin(\omega_v t - \delta_p) = \omega_v^2 B_p [\sin(\omega_v t) \cos \delta_p - \sin \delta_p \cos(\omega_v t)]$$

$$B_p \left\{ (\omega_0^2 - \omega_v^2) [\sin(\omega_v t) \cos \delta_p - \cos(\omega_v t) \sin \delta_p] + \omega_v \beta [\cos(\omega_v t) \cos \delta_p + \sin(\omega_v t) \sin \delta_p] \right\} = \frac{F_0}{m} \sin(\omega_v t); \quad \forall t$$

$$a) t_1 = 0: B_p \left\{ (\omega_0^2 - \omega_v^2) \sin \delta_p + \omega_v \beta \cos \delta_p \right\} = 0$$

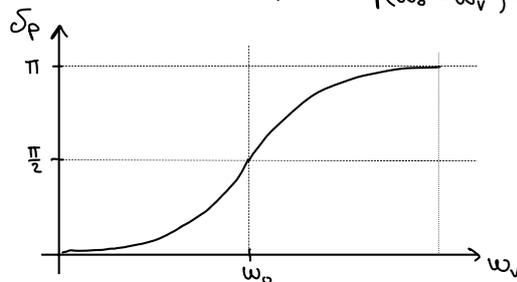
$$\begin{aligned} \nearrow \\ \sin(\omega_v t_1) = 0 \\ \cos(\omega_v t_1) = 1 \end{aligned}$$

$$\Rightarrow \tan \delta_p = \frac{\omega_v \beta}{\omega_0^2 - \omega_v^2}$$

$$\Rightarrow \cos \delta_p = \pm \frac{(\omega_0^2 - \omega_v^2)}{\sqrt{(\omega_0^2 - \omega_v^2)^2 + \omega_v^2 \beta^2}}$$

in

$$\sin \delta_p = \pm \frac{\omega_v \beta}{\sqrt{(\omega_0^2 - \omega_v^2)^2 + \omega_v^2 \beta^2}}$$



$$\omega_v \rightarrow 0: \tan \delta_p \rightarrow +0: \delta_p \rightarrow 0$$

$$\omega_v \nearrow \omega_0: \tan \delta_p \rightarrow \infty: \delta_p \nearrow \frac{\pi}{2}$$

$$\omega_v \searrow \omega_0: \tan \delta_p \rightarrow -\infty: \delta_p \searrow \frac{\pi}{2}$$

$$\omega_v \rightarrow \infty: \tan \delta_p \rightarrow -0: \delta_p \nearrow \pi$$

$$\cos \delta_p: \omega_v \rightarrow 0 \Rightarrow \delta_p \rightarrow 0: \cos \delta_p \rightarrow +1$$

$$\sin \delta_p: \delta_p \in [0, \pi] \Rightarrow \sin \delta_p > 0$$

$$b) t_2: \omega_v t_2 = \frac{\pi}{2} \Rightarrow \sin(\omega_v t_2) = 1, \cos(\omega_v t_2) = 0$$

$$\begin{aligned} & B_p \left\{ (\omega_0^2 - \omega_v^2) \cos \delta_p + \beta \omega_v \sin \delta_p \right\} = \frac{F_0}{m} \\ \text{vstavimo} & \downarrow \\ \text{sin in cos} & \left\{ \frac{(\omega_0^2 - \omega_v^2)^2 + \beta^2 \omega_v^2}{\sqrt{(\omega_0^2 - \omega_v^2)^2 + \beta^2 \omega_v^2}} \right\} = \frac{F_0}{m} \end{aligned}$$

$$\Rightarrow B_p \sqrt{(\omega_0^2 - \omega_v^2)^2 + \beta^2 \omega_v^2} = \frac{F_0}{m}$$

$$\Rightarrow B_p = \frac{F_0}{m \sqrt{(\omega_0^2 - \omega_v^2)^2 + \beta^2 \omega_v^2}} = \frac{F_0}{m \omega_v} \sqrt{\frac{\omega_v^2}{\omega_0^2 - \omega_v^2 + \beta \omega_v}}$$

$$|z| = \frac{F_0}{B_p(m\omega_v)} = \sqrt{\frac{(\omega_0^2 - \omega_v^2)^2}{\omega_v^2} + \beta^2} \leftarrow \text{absolutna vrednost impedance}$$

$$z = |z|e^{i\delta_p} \leftarrow \text{IMPEDANCA}$$

Kakšen naj bo ω_v , da bo B_p maksimalne vrednosti?

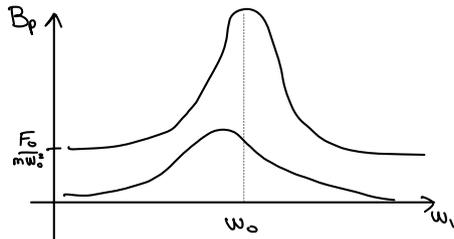
$$\text{glejamo: } (\omega_0^2 - \omega_v^2)^2 + \omega_v^2 \beta^2 = \min.$$

$$\frac{d}{d\omega_v}: 2(\omega_0^2 - \omega_v^2)(-2\omega_v) + 2\omega_v \beta^2 = 0$$

$$-2\omega_0^2 + 2\omega_v^2 + \beta^2 = 0$$

$$\Rightarrow \omega_v^2 = \omega_0^2 - \frac{\beta^2}{2}$$

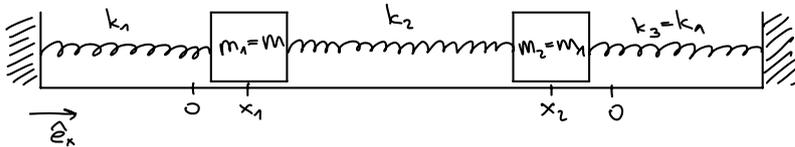
$$\Rightarrow \omega_v = \sqrt{\omega_0^2 - \frac{\beta^2}{2}} = \omega_0 \sqrt{1 - \frac{\beta^2}{2\omega_0^2}}$$



SKLOPLJENO NIHANJE

DVA SKLOPLJENA VOZIČKA NA ZRAČNI KLOPI

(1) simetričen primer:



$$\vec{F}_{1 \rightarrow 1,r} = -k_1 \Delta l_{1,r} \hat{e}_x$$

↑ sila 1. vzmeti na 1. voziček v ravnovesju

$$\vec{F}_{2 \rightarrow 1,r} = +k_2 \Delta l_{2,r} \hat{e}_x$$

↙ absolutna evakci

$$\vec{F}_{2 \rightarrow 2,r} = -k_2 \Delta l_{2,r} \hat{e}_x$$

$$\vec{F}_{3 \rightarrow 2,r} = +k_1 \Delta l_{2,r} \hat{e}_x$$

k_3

$$x_1, x_2 = 0: \vec{F}_{1 \rightarrow 1,r} + \vec{F}_{2 \rightarrow 1,r} = 0 \quad \text{in} \quad \vec{F}_{2 \rightarrow 2,r} + \vec{F}_{3 \rightarrow 2,r} = 0$$

Oba vozička zmaknemo iz ravnovesne lege:

$$x_1, x_2: \vec{F}_{1 \rightarrow 1} = \vec{F}_{1 \rightarrow 1,r} - k_1 x_1 \hat{e}_x \leftarrow \text{evakci kot v primeru enega vozička}$$

$$\vec{F}_{2 \rightarrow 1} = \vec{F}_{2 \rightarrow 1,r} - k_2 (x_1 - x_2) \hat{e}_x$$

$$\vec{F}_{1 \rightarrow 1} + \vec{F}_{2 \rightarrow 1} = m \ddot{x}_1 \hat{e}_x$$

$$\vec{F}_{1 \rightarrow 1r} - k_1 x_1 \hat{e}_x + \vec{F}_{2 \rightarrow 1r} - k_2 (x_1 - x_2) \hat{e}_x = m \ddot{x}_1 \hat{e}_x$$

$$\left[m \ddot{x}_1 + k_1 x_1 + k_2 (x_1 - x_2) \right] \hat{e}_x = 0$$

$$\Rightarrow \ddot{x}_1 + \omega_1^2 x_1 + \omega_2^2 (x_1 - x_2) = 0 \quad ; \quad \omega_1^2 = \frac{k_1}{m}, \quad \omega_2^2 = \frac{k_2}{m}$$

Podobno:

$$\Rightarrow \ddot{x}_2 + \omega_1^2 x_2 - \omega_2^2 (x_1 - x_2) = 0 \quad (k_3 = k_1, m_2 = m_1)$$

$$\left. \begin{aligned} x_a &= x_1 + x_2 \\ x_b &= x_1 - x_2 \end{aligned} \right\} \Rightarrow \begin{aligned} x_1 &= \frac{x_a + x_b}{2} \\ x_2 &= \frac{x_a - x_b}{2} \end{aligned}$$

Sestavimo (1) in (2):

$$\ddot{x}_1 + \ddot{x}_2 + \omega_1^2 (x_1 - x_2) = 0$$

$$(x_1 + x_2) + \omega_1^2 (x_1 - x_2) = 0$$

$$\Rightarrow \ddot{x}_a + \omega_a^2 x_a = 0 \quad ; \quad \omega_a^2 = \omega_1^2$$

Odštejemo (1) in (2):

$$\Rightarrow \ddot{x}_b + \omega_b^2 x_b = 0 \quad ; \quad \omega_b^2 = \omega_1^2 + 2\omega_2^2$$

nesklopljeni enačbi

$$\begin{aligned} x_a &= B_a \sin(\omega_a t + \delta_a) \\ x_b &= B_b \sin(\omega_b t + \delta_b) \end{aligned}$$

$$\Rightarrow \begin{aligned} x_1 &= C_1 \sin(\omega_a t + \delta_a) + C_2 \sin(\omega_b t + \delta_b) \\ x_2 &= C_1 \sin(\omega_a t + \delta_a) - C_2 \sin(\omega_b t + \delta_b) \end{aligned} \quad ; \quad C_1 = \frac{B_a}{2}, \quad C_2 = \frac{B_b}{2}$$

$$C_1, C_2, \delta_a, \delta_b \text{ iz začetnih pogojev: } \begin{aligned} x_1(t=0), \quad \dot{x}_1(t=0) \\ x_2(t=0), \quad \dot{x}_2(t=0) \end{aligned}$$

Primer:

$$\begin{aligned} x_1(t=0) &= x_0 \quad ; \quad \dot{x}_1(t=0) = 0 \\ x_2(t=0) &= 0 \quad \quad \dot{x}_2(t=0) = 0 \end{aligned}$$

$$\begin{aligned} \dot{x}_1 &= C_1 \omega_a \cos(\omega_a t + \delta_a) + C_2 \omega_b \cos(\omega_b t + \delta_b) \\ \dot{x}_2 &= C_1 \omega_a \cos(\omega_a t + \delta_a) - C_2 \omega_b \cos(\omega_b t + \delta_b) \end{aligned}$$

$$\begin{aligned} x_0 &= C_1 \sin \delta_a + C_2 \sin \delta_b \\ 0 &= C_1 \sin \delta_a - C_2 \sin \delta_b \end{aligned}$$

$$\begin{aligned} 0 &= C_1 \omega_a \cos \delta_a + C_2 \omega_b \cos \delta_b \\ 0 &= C_1 \omega_a \cos \delta_a - C_2 \omega_b \cos \delta_b \end{aligned}$$

$$\left. \begin{aligned} 2C_1 \omega_a \cos \delta_a &= 0 \\ 2C_2 \omega_b \cos \delta_b &= 0 \end{aligned} \right\} \Rightarrow \begin{aligned} \cos \delta_a &= 0 \Rightarrow \delta_a = \pm \frac{\pi}{2} \\ \cos \delta_b &= 0 \Rightarrow \delta_b = \pm \frac{\pi}{2} \end{aligned}$$

$$(1) \quad \delta_a = \delta_b = \frac{\pi}{2} :$$

$$\Rightarrow \sin \delta_a = 1 = \sin \delta_b$$

$$x_0 = C_1 + C_2$$

$$0 = C_1 - C_2$$

$$\left. \begin{aligned} x_0 &= C_1 + C_2 \\ 0 &= C_1 - C_2 \end{aligned} \right\} \Rightarrow C_1 = C_2 = \frac{x_0}{2}$$

$$\Rightarrow x_1 = \frac{x_0}{2} [\cos(\omega_a t) + \cos(\omega_b t)] = x_0 \cos\left(\frac{\omega_a + \omega_b}{2} t\right) \cos\left(\frac{\omega_a - \omega_b}{2} t\right)$$

$$x_2 = \frac{x_0}{2} [\cos(\omega_a t) - \cos(\omega_b t)] = x_0 \sin\left(\frac{\omega_a + \omega_b}{2} t\right) \sin\left(\frac{\omega_a - \omega_b}{2} t\right)$$

Šibka sklopitev: $k_2 \ll k_1 \Rightarrow \omega_2 = \frac{k_2}{m} \ll \omega_1 = \frac{k_1}{m}$

$$\omega_b = \sqrt{\omega_1^2 + 2\omega_2^2} = \omega_1 \sqrt{1 + 2\frac{\omega_2^2}{\omega_1^2}} \sim \omega_1 \sqrt{1 + 2\left(\frac{\omega_2}{\omega_1}\right)^2} = \omega_1 + \omega_1 \frac{\omega_2^2}{\omega_1^2}$$

$$\Rightarrow \frac{\omega_a + \omega_b}{2} \approx \omega_1$$

$$\frac{\omega_a - \omega_b}{2} \approx \omega_1 \frac{\omega_2^2}{\omega_1^2} \ll \omega_1$$

$$\Rightarrow x_0 = x_0 \cos(\omega_1 t) \cos\left(\omega_1 \frac{\omega_2^2}{\omega_1^2} t\right)$$

LASTNA NIHANJA SESTAVLJENEGA NIHALA

$$\left. \begin{aligned} x_1 &= B_1 \sin(\omega_2 t + \delta_a) + B_2 \sin(\omega_b t + \delta_b) \\ x_2 &= B_1 \sin(\omega_2 t + \delta_a) - B_2 \sin(\omega_b t + \delta_b) \end{aligned} \right\} \Rightarrow \begin{aligned} x_1 &= B_1 \sin(\omega_2 t + \delta_1) \\ x_2 &= B_2 \sin(\omega_b t + \delta_2) \end{aligned} ; \nu_c = \frac{\omega_c}{2\pi}$$

Osnovni enačbi:

$$\left. \begin{aligned} \ddot{x}_1 + \omega_1^2 x_1 + \omega_2^2 (x_1 - x_2) &= 0 ; \omega_1^2 = \frac{k_1}{m} \\ \ddot{x}_2 + \omega_1^2 x_2 - \omega_2^2 (x_1 - x_2) &= 0 ; \omega_2^2 = \frac{k_2}{m} \end{aligned} \right\}$$

Nastavek: $\left. \begin{aligned} x_1 &= C e^{i\lambda t} \\ x_2 &= D e^{i\lambda t} \end{aligned} \right\} \Rightarrow \begin{aligned} \ddot{x}_1 &= -\lambda^2 x_1 \\ \ddot{x}_2 &= -\lambda^2 x_2 \end{aligned}$

$$\left. \begin{aligned} \vec{x} = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} C \\ D \end{bmatrix} e^{i\lambda t} \\ -\lambda^2 x_1 + \omega_1^2 x_1 + \omega_2^2 (x_1 - x_2) = 0 \\ -\lambda^2 x_2 + \omega_1^2 x_2 + \omega_2^2 (x_1 - x_2) = 0 \end{aligned} \right\} \Rightarrow \begin{bmatrix} \omega_1^2 + \omega_2^2 - \lambda^2 & -\omega_2^2 \\ -\omega_2^2 & \omega_1^2 + \omega_2^2 - \lambda^2 \end{bmatrix} \begin{bmatrix} C \\ D \end{bmatrix} e^{i\lambda t} = 0 ; \forall t$$

$$\begin{bmatrix} \omega_1^2 + \omega_2^2 - \lambda^2 & -\omega_2^2 \\ -\omega_2^2 & \omega_1^2 + \omega_2^2 - \lambda^2 \end{bmatrix} \begin{bmatrix} C \\ D \end{bmatrix} = 0$$

$$\Rightarrow (\omega_1^2 + \omega_2^2 - \lambda^2)^2 - \omega_2^2 \omega_2^2 = 0 \quad (C, D, \lambda = ?)$$

$$\omega_1^2 + \omega_2^2 - \lambda^2 = \pm \omega_2^2$$

a) +: $\lambda^2 = \omega_1^2 \Rightarrow \lambda = \pm \omega_1 = \pm \omega_a$

b) -: $\omega_1^2 + 2\omega_2^2 = \lambda^2 \Rightarrow \lambda = \pm \omega_b$

a) $\lambda = \pm \omega_a$: $\begin{aligned} +): & \begin{aligned} x_1 &= C_1 e^{i\omega_1 t} \\ x_2 &= D_1 e^{i\omega_1 t} \end{aligned} \\ & \begin{bmatrix} \omega_2^2 & -\omega_2^2 \\ -\omega_2^2 & \omega_2^2 \end{bmatrix} \begin{bmatrix} C_1 \\ D_1 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix} \end{aligned}$

$$\left. \begin{aligned} \omega_2^2 (C_1 - D_1) &= 0 \\ -\omega_2^2 (C_1 - D_1) &= 0 \end{aligned} \right\} \Rightarrow C_1 = D_1$$

dobimo vsa enak način
-): $C_2 = D_2$: $\begin{aligned} x_1 &= C_2 e^{-i\omega_1 t} \\ x_2 &= D_2 e^{-i\omega_1 t} \end{aligned}$

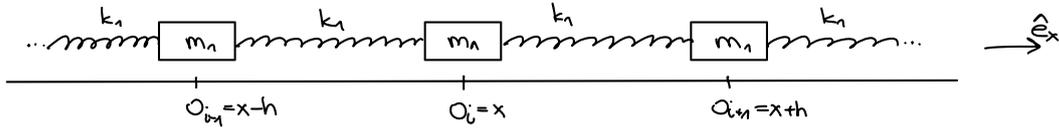
$$\Rightarrow \begin{aligned} x_1 &= C_1 e^{i\omega_1 t} + C_2 e^{-i\omega_1 t} \\ x_2 &= C_1 e^{i\omega_1 t} + C_2 e^{-i\omega_1 t} \end{aligned}$$

$$\Rightarrow \begin{aligned} x_1 &= (C_1 + C_2) \cos(\omega_1 t) + i(C_1 - C_2) \sin(\omega_1 t) = B_1 \sin(\omega_2 t + \delta_1) \quad \forall t \\ x_2 &= x_1 = B_2 \sin(\omega_2 t + \delta_2) \quad \forall t \end{aligned}$$

$$\left. \begin{aligned} \text{(i)} \quad t_1=0 : C_1+C_2 &= B_1 \sin \delta_1 \\ C_1+C_2 &= B_2 \sin \delta_2 \\ B_1 \sin(\omega_2 t + \delta_1) &= B_2 \sin(\omega_2 t + \delta_2) \end{aligned} \right\} \Rightarrow B_1 = B_2 \text{ in } \delta_1 = \delta_2$$

MEHANSKO VALOVANJE - VALOVNA ENAČBA

DISKRETNI MODEL MASIVNE VZMETI:



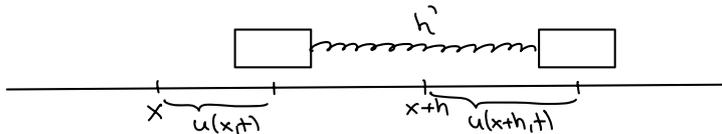
l ... skupna dolžina vzmeti
 $nm_1 = m$... masa vzmeti
 k ... koeficient celotne vzmeti

$$n = \frac{l}{h}, \quad m_1 = \frac{m}{n}, \quad k_1 = k \frac{l}{h}$$

$x \mapsto u(x,t)$... odmik uteži z ravnovesno lego v x od ravnovesne lege ob času t v smeri \hat{e}_x

$$x \neq x(t) \quad \text{oz. } \dot{x} = 0$$

↑ ravnovesna lega se s časom ne spreminja



$$u(x,t) + h' = h + u(x+h,t)$$

$$\Rightarrow h' - h = \Delta h = u(x+h,t) - u(x,t)$$

$$\Rightarrow \left. \begin{aligned} F_{i+1 \rightarrow i} &= F_{i+1 \rightarrow i,r} + k_1 [u(x+h,t) - u(x,t)] \\ F_{i-1 \rightarrow i} &= F_{i-1 \rightarrow i,r} - k_1 [u(x,t) - u(x-h,t)] \end{aligned} \right\} \Rightarrow F_{i+1 \rightarrow i,r} + F_{i-1 \rightarrow i,r} = 0$$

$$\Rightarrow F_i = F_{i+1 \rightarrow i} + F_{i-1 \rightarrow i} = k_1 \left[\frac{u(x+h,t) - u(x,t)}{h} - \frac{u(x,t) - u(x-h,t)}{h} \right] =$$

↑ skupna sila na telo i

$$= k l \left[\frac{u(x+h,t) - u(x,t)}{h} - \frac{u(x,t) - u(x-h,t)}{h} \right]$$

$$F_i = m_1 \frac{d^2 u(x,t)}{dt^2} \quad (\text{2. Newtonov zakon})$$

$$\frac{du(x,t)}{dt} = \frac{\partial u}{\partial t} + \frac{\partial u}{\partial x} \frac{\partial x}{\partial t} = \frac{\partial u}{\partial t}$$

$\dot{x} = 0$

$$\Rightarrow \frac{d^2 u}{dt^2} = \frac{d}{dt} \left(\frac{\partial u}{\partial t} \right) = \frac{\partial^2 u}{\partial t^2} + \frac{\partial^2 u}{\partial x \partial t} \dot{x} = \frac{\partial^2 u}{\partial t^2}$$

$$\Rightarrow F_i = m_1 \frac{\partial^2 u}{\partial t^2}; \quad m_1 = \frac{m}{n} = \frac{m}{l} h$$

$$\frac{m}{l} \frac{\partial^2 u}{\partial t^2} = k l \frac{\frac{u(x+h,t) - u(x,t)}{h} - \frac{u(x,t) - u(x-h,t)}{h}}{h}$$

$$\Rightarrow \frac{\partial^2 u}{\partial t^2} = \frac{k l^2}{m} \frac{\frac{u(x+h,t) - u(x,t)}{h} - \frac{u(x,t) - u(x-h,t)}{h}}{h}$$

ni nujno da obstaja limita tega

$$n \rightarrow \infty \Leftrightarrow h \rightarrow 0 : \frac{\frac{\partial u(x,t)}{\partial x} - \frac{\partial u(x-h,t)}{\partial x}}{h} \Rightarrow \frac{\partial^2 u(x,t)}{\partial x^2}$$

$$\Rightarrow \boxed{\frac{\partial^2 u}{\partial t^2} = c^2 \frac{\partial^2 u}{\partial x^2}} \leftarrow \text{VALOVNA ENAČBA}$$

$$c^2 = \frac{kl^2}{m} \quad \left[\frac{m}{s} \right]$$

VALOVANJE PO ELASTIČNI PALICI:

$$\frac{\Delta F}{S} = -E \frac{\Delta l}{l}; \quad [E] = \frac{N}{m^2} \quad \begin{array}{l} \text{YOUNGOV} \\ \text{ELASTIČNI MODUL} \end{array}$$

$$\Delta l \propto \frac{1}{E}$$

$$\Delta F = - \underbrace{\frac{ES}{l}}_k \Delta l = k \Delta l \quad \boxed{c^2 = \frac{kl^2}{m} = \frac{ESl^2}{lm} = \frac{ESl}{m} = \frac{E \cdot v}{\rho} = \frac{E}{\rho}}$$

$$\Delta F > 0, \Delta l < 0$$

TEKOČINA, ZAPRTA V DOLGI TANKI CEVI:

$$\begin{array}{l} \leftarrow \text{viskoznost} \\ \eta \rightarrow 0 \\ S = \text{konst.} \end{array}$$

$$\Delta p = -\frac{1}{\chi} \frac{\Delta V}{V}; \quad \Delta V = -\chi V \Delta p$$

$$\Delta p > 0 \Rightarrow \Delta V < 0$$

$$\Delta p < 0 \Rightarrow \Delta V > 0$$

$$\frac{\Delta F}{S} = -\frac{1}{\chi} \frac{\Delta V}{V}$$

$$\Delta F = \frac{S}{\chi V} \Delta V; \quad \Delta V = S \Delta l$$

$$\Rightarrow \Delta F = -\frac{SS \Delta l}{\chi S l}$$

$$\Delta F = -\frac{S}{\chi l} \Delta l = k \cdot \Delta l$$

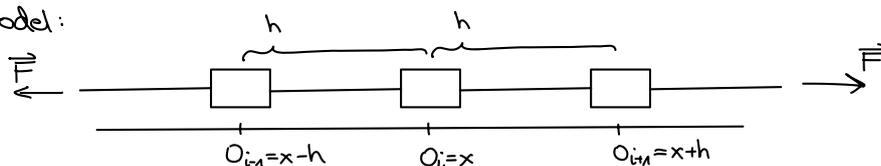
$$\boxed{c^2 = \frac{kl^2}{m} = \frac{S l^2}{\chi l m} = \frac{S l}{\chi m} = \frac{V}{\chi m} = \frac{1}{\chi S}}$$

Do sedaj: $u(x,t)$ v smeri \hat{e}_x (smer potovanja motnje) \Rightarrow LONGITUDINALNO VALOVANJE

VALOVANJE PO NAPETI VRVI:

$$u(x,t) \perp \hat{e}_x$$

Diskretni model:



$u(x,t)$: odmik $(i-k)$ -te uteži od ravnovesne lege ob času t v smeri \hat{e}_y

$$\Rightarrow \boxed{\frac{\partial^2 u(x,t)}{\partial t^2} = c^2 \frac{\partial^2 u(x,t)}{\partial x^2}; \quad c^2 = \frac{F}{\mu}}$$

VALOVNA ENAČBA V 3 DIMENZIJAH:

$$\frac{\partial^2}{\partial x^2} \rightarrow \nabla^2 \equiv \left(\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2} \right)$$

$$\Rightarrow \boxed{\frac{\partial^2 u}{\partial t^2} = c^2 \nabla^2 u}$$

Definiramo: $\square \equiv \frac{1}{c^2} \frac{\partial^2}{\partial t^2} - \nabla^2$

$$\square u = 0$$

REŠITVE 1-DIMENZIONALNE VALOVNE ENAČBE

dvakrat odvedljiva $f(x-ct)$

$$u(x,t) = f(x-ct); \quad \eta \equiv x-ct$$

$$\Rightarrow u = f(\eta(x,t))$$

$$\Rightarrow \frac{\partial u}{\partial t} = \frac{\partial u}{\partial \eta} \frac{\partial \eta}{\partial t} = -c \frac{\partial u}{\partial \eta}$$

$$\frac{\partial}{\partial t} \left(\frac{\partial u}{\partial \eta} \right) = \frac{\partial}{\partial \eta} \left(\frac{\partial u}{\partial \eta} \right) \frac{\partial \eta}{\partial t}$$

$$\Rightarrow \frac{\partial^2 u}{\partial t^2} = \frac{\partial}{\partial t} \left(-c \frac{\partial u}{\partial \eta} \right) = -c \frac{\partial}{\partial t} \left(\frac{\partial u}{\partial \eta} \right) = -c \frac{\partial}{\partial \eta} \left(\frac{\partial u}{\partial \eta} \right) \frac{\partial \eta}{\partial t} = c^2 \frac{\partial^2 u}{\partial \eta^2}$$

$$\Rightarrow \frac{\partial^2 u}{\partial x^2} = \frac{\partial^2 u}{\partial \eta^2} \Rightarrow \frac{\partial^2 u}{\partial t^2} = c^2 \frac{\partial^2 u}{\partial x^2}$$

INTERPRETACIJA REŠITVE:

Velja:

- a) $u(x,t) = u(x-ct, 0)$
- b) $u(x,t) = u(0, t-\frac{x}{c})$

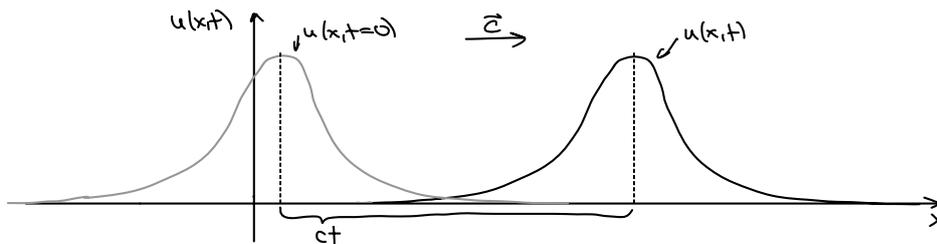
* velja tudi: $u(x,t) = g(x+ct)$
 $\Rightarrow u(x,t) = u_1(x,t) + u_2(x,t)$ tudi rešitev

$$u(x,t) = f(x-ct):$$

- a) $u(x-ct, 0) = f(x-ct-c \cdot 0) = f(x-ct) = u(x,t)$
- b) $u(0, t-\frac{x}{c}) = f(0-c(t-\frac{x}{c})) = f(-ct+x) = f(x-ct) = u(x,t)$

k a):

$u(x,t)$... odmik od ravnovesne lege ob času t
 $u(x-ct, 0)$... odmik točke iz ravnovesne lege $x-ct$ ob času 0



t : motnja prepotuje razdaljo $ct = \Delta x$

$\Rightarrow c$... hitrost potovanja motnje/valovanja

c : v splošnem ni enaka hitrosti v ($v = \left| \frac{du}{dt} \right|_{x=0} = \left| \frac{\partial u}{\partial t} \right| = \left| \frac{\partial u}{\partial \eta} \frac{\partial \eta}{\partial t} \right| = c \left| \frac{\partial u}{\partial \eta} \right|_{x_1} \Rightarrow v \neq c$)

(a) \Rightarrow val točno določen iz začetnega pogoja

(b): če poznamo $u(x=0, t)$, lahko določimo $u(x, t)$
 \Rightarrow val določen iz robnega pogoja

* $u(x, t) = u_1(x, t) + u_2(x, t)$ tudi rešitev $\frac{\partial^2 u}{\partial t^2} = c^2 \frac{\partial^2 u}{\partial x^2}$

$$\frac{\partial^2}{\partial t^2} (u_1 + u_2) = \frac{\partial^2 u_1}{\partial t^2} + \frac{\partial^2 u_2}{\partial t^2} = c^2 \frac{\partial^2 u_1}{\partial x^2} + c^2 \frac{\partial^2 u_2}{\partial x^2}$$

$$\frac{\partial^2}{\partial x^2} (u_1 + u_2) = \frac{\partial^2 u_1}{\partial x^2} + \frac{\partial^2 u_2}{\partial x^2}$$

$$u(x, t) = f(x-ct) + g(x+ct)$$

Dva začetna pogoja (d'Alembert)

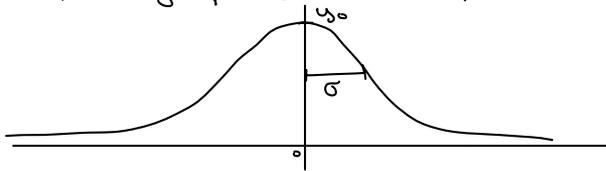
$$u(x, 0) = f(x) + g(x) = A(x)$$

$$\left. \frac{\partial u(x, t)}{\partial t} \right|_{t=0} = B(x)$$

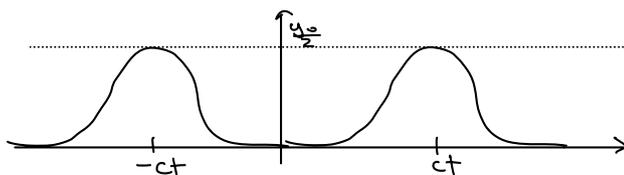
$$u(x, t) = \frac{1}{2} [A(x-ct) + A(x+ct)] + \frac{1}{2c} \int_{x-ct}^{x+ct} B(x) dx$$

Primer:

$$u(x, t=0) = u_0 \exp\left\{-\frac{x^2}{2\sigma^2}\right\} = A(x) ; \quad 0 = B(x)$$



$$u(x, t) = \frac{u_0}{2} \left[\exp\left\{-\frac{(x-ct)^2}{2\sigma^2}\right\} + \exp\left\{-\frac{(x+ct)^2}{2\sigma^2}\right\} \right]$$



POTUJOČE SINUSNO VALOVANJE

$$u(x, t) = f(x-ct)$$

a) $u(x, t) = u(x-ct, 0)$ (začetni pogoji)

b) $u(x, t) = u(0, t - \frac{x}{c})$ (robni pogoji)

$$u(x=0, t) = u_0 \sin(-\omega t + \delta) ; \quad \forall t$$

$$u(x, t) = u(0, t - \frac{x}{c}) = u_0 \sin[-\omega(t - \frac{x}{c}) + \delta] = u_0 \sin\left(\frac{\omega}{c}x - \omega t + \delta\right) = u_0 \sin(kx - \omega t + \delta)$$

$$k = \frac{\omega}{c} = \frac{2\pi\nu}{c} \quad \left[\frac{1}{m} \right]$$

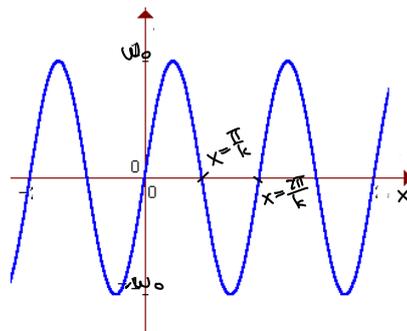
\nwarrow VALOVNO ŠTEVILO

Primer: $\delta=0$: slikamo ob času $t=0$
 $u(x,t=0) = u_0 \sin(kx)$

$$\lambda = \frac{2\pi}{k}$$

$$\Rightarrow k = \frac{2\pi}{\lambda} = \frac{2\pi\nu}{c}$$

$$\Rightarrow \boxed{c = \lambda\nu}$$



(valovanje v drugo smer: $u(x,t) = g(x+ct)$)

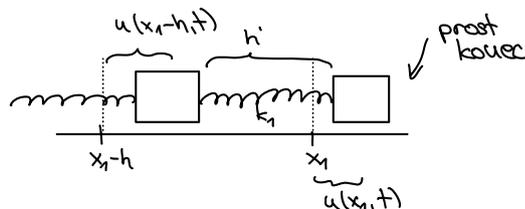
ROBNI POGOJI IN STOJNO/STOJEČE SINUSNO VALOVANJE

ROBNI POGOJI:

a) $u(x_1,t) = 0$ (togo vpet konec)

b) $\frac{\partial u}{\partial x}(x,t) = 0$ (prost konec)

MODEL DISKRETNE MASIVNE VZMETI:



$$u(x_1-h,t) + h = h + u(x_1,t)$$

$$\Delta h = h' - h = u(x_1,t) - u(x_1-h,t)$$

$$F_{x_1-h \rightarrow x_1} = \underbrace{F_{x_1-h \rightarrow x_1}}_0 - k_1 \Delta h = -k_1 \Delta h = -\frac{k\ell}{n} (u(x_1,t) - u(x_1-h,t)) = F_{x_1}$$

$$2. \text{ Newtonov zakon: } \boxed{F_{x_1} = m_1 \frac{\partial^2 u(x,t)}{\partial t^2} = \frac{m_1}{n} \frac{\partial^2 u}{\partial t^2} = \frac{m}{L} \frac{\partial^2 u}{\partial t^2} = \frac{mh}{L} \frac{\partial^2 u}{\partial t^2}}$$

$$\Rightarrow -\frac{k\ell^2}{m} \frac{u(x,t) - u(x-h,t)}{h} = h \frac{\partial^2 u}{\partial t^2}$$

$$n \rightarrow \infty, h \rightarrow 0: -c^2 \frac{\partial u(x,t)}{\partial x} \Big|_{x=x_1} = 0 \Rightarrow \boxed{\frac{\partial u(x,t)}{\partial x} \Big|_{x=x_1} = 0}$$

PALICA PROSTA NA OBEH KONCIH:

$$\frac{\partial u}{\partial x}(x,t) \Big|_{x=0} = 0 \text{ in } \frac{\partial u}{\partial x}(x,t) \Big|_{x=L} = 0; L \dots \text{ dolžina palice}$$



Predpostavimo: $u(x,t) = u_0 \sin(kx - \omega t + \delta_1) + u_0 \sin(kx + \omega t + \delta_2)$

$$\frac{\partial u}{\partial x}(x,t) = u_0 k [\cos(kx - \omega t + \delta_1) + \cos(kx + \omega t + \delta_2)] =$$

$$= 2u_0 k \cos(kx + \frac{\delta_1 + \delta_2}{2}) \cos(-\omega t + \frac{\delta_1 - \delta_2}{2})$$

$$a) x=0: 2u_0 k \cos(\frac{\delta_1 + \delta_2}{2}) \cos(-\omega t + \frac{\delta_1 - \delta_2}{2}) = 0, \forall t \Rightarrow \frac{\delta_1 + \delta_2}{2} = \frac{\pi}{2}$$

$$\cos(kx + \frac{\delta_1 + \delta_2}{2}) = \cos(kx + \frac{\pi}{2}) = \sin(kx)$$

$$x=L: 2u_0 k \sin(kL) \cos(-\omega t + \frac{\delta_1 - \delta_2}{2}) = 0, \forall t \Rightarrow kL = n\pi, n \in \mathbb{Z}$$

$$\Rightarrow k_n = \frac{n\pi}{L}$$

$$k_n = \frac{2\pi}{\lambda_n} = \frac{n\pi}{L} \Rightarrow \frac{2}{\lambda_n} = \frac{n}{L}$$

$$\Rightarrow \lambda_n = \frac{2L}{n} = \frac{1}{\lambda_n}$$

$$\lambda_n v_n = c \Rightarrow v_n = \frac{nc}{2L}$$

$$u(x,t) = 2u_0 \sin(kx + \frac{\delta_1 + \delta_2}{2}) \cos(-\omega t + \frac{\delta_1 - \delta_2}{2}) =$$

$$= 2u_0 \sin(kx + \frac{\pi}{2}) \cos(\omega t + \frac{\delta_2 - \delta_1}{2}) =$$

$$= 2u_0 \cos(kx) \cos(\omega t + \frac{\delta_2 - \delta_1}{2}) ; k_n = \frac{\omega_n}{c}$$

Primer: $\frac{\delta_2 - \delta_1}{2} = 0$

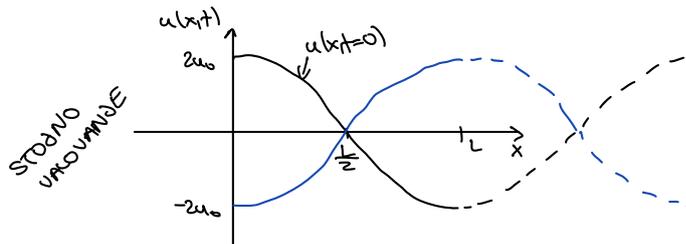
$$\Rightarrow u(x,t) = 2u_0 \cos(k_n x) \cos(\omega t)$$

$t=0:$

$$n=1: k_1 = \frac{\pi}{L} \Rightarrow \cos(k_1 x) = \cos(\frac{\pi x}{L}); x=0 \Rightarrow \cos(\frac{\pi}{L} \cdot 0) = 1$$

$$x=L \Rightarrow \cos(\frac{\pi}{L} \cdot L) = -1$$

$$x=\frac{L}{2} \Rightarrow \cos(\frac{\pi}{L} \cdot \frac{L}{2}) = 0$$



Primer:



$$x < 0: u_1(x,t) = f_1(x - c_1 t) + g_1(x + c_1 t) \leftarrow \text{zamenja smer/se odbije}$$

$$x \geq 0: u_2(x,t) = f_2(x - c_2 t)$$

odbojnost: $\frac{|g_1|}{|f_1|} = \frac{|c_1 - c_2|}{c_1 + c_2}$; $c_2 = 0 \Rightarrow \frac{|g_1|}{|f_1|} = 1$ } vse se odbije

prepustnost: $\frac{|f_2|}{|f_1|} = \frac{2c_2}{c_1 + c_2}$; $c_2 = 0 \Rightarrow \frac{|f_2|}{|f_1|} = 0$

$$u_1(x=0,t) = u_2(x=0,t) \quad (\text{palica se ne strga})$$

$$\frac{\partial u_1}{\partial x}(x=0,t) = \frac{\partial u_2}{\partial x}(x=0,t)$$

ENERGIJA VALOVANJA

Potovanje motnje \rightarrow potovanje energije

diskretni model vzmeti: $W_k; W_{pr}$

uteži na položaju x

$$x: W_k = \frac{1}{2} m_1 v^2$$

$$= \frac{1}{2} m_1 \left(\frac{du(x,t)}{dt} \right)^2$$

$$= \frac{1}{2} m_1 \left(\frac{\partial u(x,t)}{\partial t} \right)^2$$

$$= \frac{1}{2} \frac{m\Delta x}{L} \left(\frac{\partial u(x,t)}{\partial t} \right)^2$$

$$\Rightarrow \frac{W_k}{n} = \frac{1}{2} \frac{m}{L} \left(\frac{\partial u(x,t)}{\partial t} \right)^2 \leftarrow \text{kinetična energija posamezne uteži}$$

; h... razdalja med sosednjima utežema v ravnovesju

$$W_{pr} = \frac{1}{2} k_1 (\Delta h)^2 = \frac{1}{2} k_1 [u(x+h,t) - u(x,t)]^2 = \frac{1}{2} \frac{kL}{n} [u(x+h,t) - u(x,t)]^2 = \frac{1}{2} kLh \left[\frac{u(x+h,t) - u(x,t)}{h} \right]^2$$

$$\Rightarrow \frac{W_{pr}}{n} = \frac{1}{2} kL \left[\frac{u(x+h,t) - u(x,t)}{h} \right]^2 \xrightarrow{h \rightarrow 0} \frac{1}{2} kL \left[\frac{\partial u(x,t)}{\partial x} \right]^2 \leftarrow \text{pržnostna energija}$$

$$\frac{1}{2}kl = \frac{1}{2}kl \frac{L}{m} \frac{m}{L} = \frac{1}{2} \frac{kL^2}{m} \frac{m}{L} = \frac{1}{2} c^2 \frac{m}{L}$$

$$\Rightarrow \lim_{h \rightarrow 0} \frac{W_{pr}}{h} = \frac{1}{2} c^2 \frac{m}{L} \left(\frac{\partial u(x,t)}{\partial x} \right)^2$$

Primer prožne palice: $m = \rho V = \rho S L$
 $k = \frac{ES}{L}$

$$\Rightarrow \frac{W_k}{h} = \frac{1}{2} \rho S \left(\frac{\partial u(x,t)}{\partial t} \right)^2$$

$$\Rightarrow \lim_{h \rightarrow 0} \frac{W_{pr}}{h} = \frac{1}{2} c^2 \rho S \left(\frac{\partial u(x,t)}{\partial x} \right)^2$$

GOSTOTA KINETIČNE ENERGIJE: $W_k = \frac{W_k}{\Delta V} = \frac{W_k}{hS} = \frac{1}{2} \rho \left(\frac{\partial u(x,t)}{\partial t} \right)^2$

GOSTOTA PROŽNOSTNE ENERGIJE: $W_{pr} = \frac{W_{pr}}{\Delta V} = \frac{W_{pr}}{Sh} = \frac{1}{2} c^2 \rho \left(\frac{\partial u(x,t)}{\partial x} \right)^2$

ENERGIJA SINUSNEGA VALOVANJA:

$$u(x,t) = u_0 \sin(kx - \omega t + \delta)$$

smer: \vec{e}_x

k ... VALOVNO ŠTEVILO (ne koeficient vzemati)

$$k = \frac{2\pi}{\lambda} = \frac{2\pi \nu}{\lambda \nu} = \frac{\omega}{c} \rightarrow \omega = ck$$

$$\frac{\partial u(x,t)}{\partial t} = -\omega u_0 \cos(kx - \omega t + \delta)$$

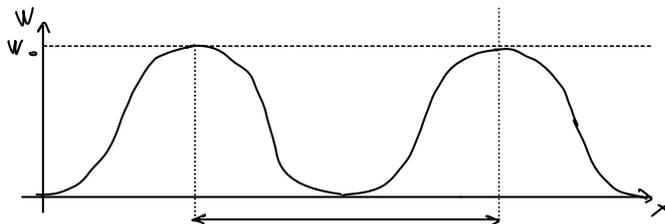
$$\frac{\partial u(x,t)}{\partial x} = k u_0 \cos(kx - \omega t + \delta)$$

$$\Rightarrow W_k = \frac{1}{2} \rho \omega^2 u_0^2 \cos^2(kx - \omega t + \delta)$$

$$W_{pr} = \frac{1}{2} c^2 \rho k^2 u_0^2 \cos^2(kx - \omega t + \delta) = \frac{1}{2} \omega^2 \rho u_0^2 \cos^2(kx - \omega t + \delta)$$

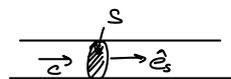
$$\Rightarrow W_{pr} = W_k$$

SKUPNA GOSTOTA: $W = W_k + W_{pr} = u_0^2 \omega^2 \rho \cos^2(kx - \omega t + \delta)$



POVPREČNA GOSTOTA: $\bar{W} = \frac{1}{2} u_0^2 \omega^2 \rho$

$$\bar{W} = \Delta V \bar{w} = ct S \bar{w}, \quad S \perp c$$



$$S \rightarrow \vec{S} = S \vec{e}_s$$

$$\vec{e}_s \parallel \vec{c}$$

P... ENERGIJSKI TOK VALOVANJA

$$P = \frac{\bar{W}}{t} = \frac{ct S \bar{w}}{t} = c S \bar{w} \quad \left[W = \frac{m}{s} m^2 \frac{m^2 k^2}{s^2 n^2} = \frac{m^2 k^2}{s^2} = N \frac{m}{s} = \frac{J}{s} \right]$$

GOSTOTA ENERGIJSKEGA TOKA: $\vec{j} = \frac{P}{S} = \bar{w} c \quad \left[\frac{W}{m^2} \right]$

Primeri: $j = 10^{-12} \frac{W}{m^2}$; $\nu = 1 \text{ kHz}$ (meja slišnosti)

$j = 1 \frac{W}{m^2}$; $\nu = 1 \text{ kHz}$ (meja bolečine)

$j = 1.4 \frac{kW}{m^2}$ (sončni tok pred vstopom v atmosfero)

Zanima nas povezava med $u(x,t)$ in Δp (tlak)

2. Newtonov zakon: $m_1 \frac{du}{dt} = F_x$ (utež v ravnovesju v legi x)

$\frac{mh}{2} \frac{\partial^2 u}{\partial t^2} = F_x$; $F_x = F_{x+h \rightarrow x} + F_{x+h \rightarrow x}$

$h \rightarrow 0$: $F_x \rightarrow 0$

$F_{x+h \rightarrow x} + F_{x+h \rightarrow x} = 0 \rightarrow |F_{x+h \rightarrow x}| = |F_{x+h \rightarrow x}|$

$F_{x+h \rightarrow x} = p \cdot S$

$\Rightarrow p = \frac{1}{S} F_{x+h \rightarrow x} = \frac{1}{S} [F_{x+h \rightarrow x,r} - k_1(u(x,t) - u(x-h,t))]$
 $= \frac{F_{x+h \rightarrow x,r}}{S} - \frac{k_1[u(x,t) - u(x-h,t)]}{S}$
RAVNOVESNI TLAK

$\Rightarrow p - p_0 = -\frac{k_1}{S} [u(x,t) - u(x-h,t)] = -\frac{k\ell}{Sh} [u(x,t) - u(x-h,t)] = -\frac{k\ell}{S} \left(\frac{u(x,t) - u(x-h,t)}{h} \right) = (*)$
razlika med trenutnim in ravnovesnim tlakom

$\frac{1}{\chi} : c^2 = \frac{E}{\rho_1} \Rightarrow \frac{1}{\chi\rho} = \frac{k\ell^2}{m} = \frac{k\ell^2}{\rho S \ell} = \frac{k\ell}{\rho S}$
 $= \frac{1}{\chi} = \frac{k\ell}{S}$

$h \rightarrow 0$
 $(*) = -\frac{1}{\chi} \frac{\partial u(x,t)}{\partial x} = p - p_0$

$u = u_0 \sin(kx - \omega t + \delta)$

$\frac{\partial u}{\partial x} = k u_0 \cos(kx - \omega t + \delta)$

$\Delta p = -\frac{k}{\chi} u_0 \cos(kx - \omega t + \delta) =$
 $= -\frac{\omega}{\chi c} u_0 \cos(kx - \omega t + \delta)$
 Δp_0 amplituda tlačne razlike

$\Delta p = \frac{\omega u_0}{\chi c} ; \omega = 2\pi \nu$
 $j = \overline{w} \cdot c = \frac{1}{2} \rho \omega^2 u_0^2$

STISLJIVOST: $\chi = -\frac{1}{V} \frac{\partial V}{\partial p}$; $\chi > 0$

a) IZOTERMNO STISKANJE IDEALNEGA PLINA

konst. = $\frac{pV}{T} = \frac{p'V'}{T}$; $p_1 V_1 T \rightarrow p_1' V_1' T'$

IZOTERMA SPREMENBA:

$$T=T' \Rightarrow pV = p'V' = \text{konst.} \rightarrow V = \frac{K}{p} \rightarrow \frac{\partial V}{\partial p} = -\frac{K}{p^2} = -\frac{1}{p} \left(\frac{K}{p}\right) = -\frac{V}{p}$$

$$\Rightarrow \chi = \frac{1}{p}$$

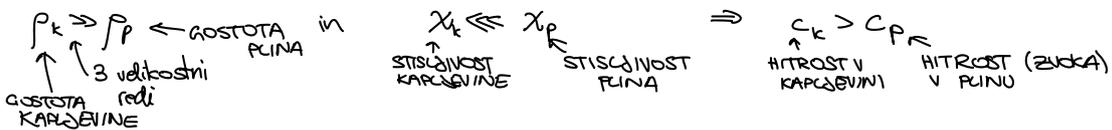
b) ADIABATNA / ENTROPNA STIŠLJIVOST

$$pV^{\kappa} = K \quad ; \quad \kappa = \frac{C_p}{C_v} = \begin{cases} \frac{5}{3} = 1.67; & \text{1-atomni plin} \\ \frac{7}{5} = 1.4; & \text{2-atomni plin} \\ \frac{4}{3} = 1.33; & \text{3-atomni plin} \end{cases}$$

$$\Rightarrow V = K \frac{1}{p^{\frac{1}{\kappa}}} \Rightarrow \frac{\partial V}{\partial p} = K \frac{1}{\kappa} \left(-\frac{1}{p}\right) \frac{1}{p} p^{-\frac{1}{\kappa}} = -\frac{V}{\kappa p}$$

$$\Rightarrow \chi = \frac{1}{\kappa p}$$

$$c = \sqrt{\frac{1}{\rho \chi}}$$



Primeri: $M_2 = 28 \text{ kg}$
 $T = 0^\circ\text{C}$
 $p = 1 \text{ bar}$
 $\kappa = 1.4$

$\Rightarrow c = ???$

$\nu = 1000 \text{ Hz}$
 $\lambda = 10^{-12} \frac{\text{W}}{\text{m}^2}$

$\Rightarrow u_0 = ???$
 $\Delta p = ???$

ZVOK V 3D (3 dimenzije)

1D: $c^2 \frac{\partial^2 u}{\partial x^2} = \frac{\partial^2 u}{\partial t^2}$

3D: $c^2 \nabla^2 \vec{u} = \frac{\partial^2 \vec{u}}{\partial t^2}$

RAVNI VAL:

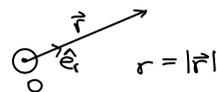
odmik od ravnovesne lege (v smeri x)
 $u(x,t) \rightarrow \vec{u}(\vec{r},t) \downarrow$
 $\vec{u}(\vec{r},t) = \vec{u}_0 \sin(kx - \omega t + \delta)$; \vec{z} v smeri \hat{e}_x

(kerato za smeri y in z)

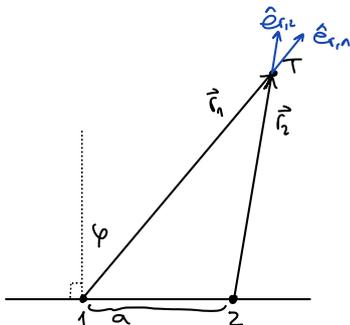
KROGLJENI VALOVANJE

$$\vec{u}(\vec{r},t) = u(\vec{r},t) \hat{e}_r$$

$$u(\vec{r},t) = \frac{u_0}{r} \sin(kr - \omega t + \delta)$$



INTERFERENCA KROGLJNEGA VALOVANJA

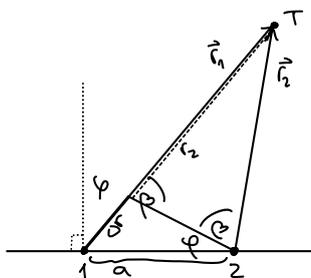


$$\vec{u}_1(\vec{r},t) = \frac{u_0}{r_1} \sin(kr_1 - \omega t + \delta_1) \hat{e}_{r_1}$$

$$\vec{u}_2(\vec{r},t) = \frac{u_0}{r_2} \sin(kr_2 - \omega t + \delta_2) \hat{e}_{r_2}$$

$$\vec{u} = \vec{u}_1(\vec{r},t) + \vec{u}_2(\vec{r},t)$$

Poseben primer: T zelo daleč od zvočnikov: $r_1, r_2 \gg a$ $\hat{e}_{r,1} = \hat{e}_{r,2} = \hat{e}_r$



$$\Delta r = r_1 - r_2 \quad \beta \approx \frac{\pi}{2}$$

$$\Delta r \approx a \sin \varphi$$

$$r_1 = \Delta r + r_2 = r_2 + a \sin \varphi = r_2 \left(1 + \frac{a}{r_2} \sin \varphi\right)$$

$$\rightarrow \frac{1}{r_1} = \frac{1}{r_2 \left(1 + \frac{a}{r_2} \sin \varphi\right)} \approx \frac{1}{r_2} \left(1 - \frac{a}{r_2} \sin \varphi\right) \approx \frac{1}{r_2}$$

$$\vec{u} = \frac{u_0}{r_2} \left[\sin(kr_1 - \omega t + \delta_1) + \sin(kr_2 - \omega t + \delta_2) \right] \hat{e}_r$$

$$u = 2 \frac{u_0}{r_2} \sin \left(k \frac{r_1 + r_2}{2} - \omega t + \frac{\delta_1 + \delta_2}{2} \right) \cos \left(k \frac{\Delta r}{2} + \frac{\delta_1 - \delta_2}{2} \right)$$

$$u = \frac{2u_0}{r_2} \sin \left(k \frac{r_1 + r_2}{2} - \omega t + \frac{\delta_1 + \delta_2}{2} \right) ; \quad \tilde{u}_0 = 2u_0 \cos \left(k \frac{\Delta r}{2} + \frac{\delta_1 - \delta_2}{2} \right)$$

Primer: $\delta_1 = \delta_2$ (zvočnika utripata istočasno)

$$\Rightarrow \frac{\delta_1 - \delta_2}{2} = 0 \Rightarrow \tilde{u}_0 = 2u_0 \cos \left(k \frac{\Delta r}{2} \right)$$

a) ojačitve: $\cos \left(k \frac{\Delta r}{2} \right) = \pm 1$

$$k \frac{\Delta r}{2} = n\pi ; n \in \mathbb{Z}$$

$$\frac{2\pi}{\lambda} \cdot \frac{a \sin \varphi}{2} = n\pi \Rightarrow a \sin \varphi = n\lambda \leftarrow \text{pogoji za ojačanje}$$

$$|n\lambda| \leq a$$

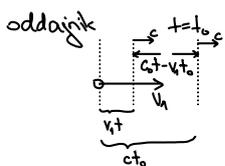
$n=0$: $\sin \varphi = 0 \Rightarrow \varphi = 0$
 $\varphi_n = \arcsin \left(\frac{n\lambda}{a} \right)$ } koti, pri katerih so ojačitve

b) oslabitve: $\cos \left(k \frac{\Delta r}{2} \right) = 0$

$$\rightarrow a \sin \varphi = \left(n + \frac{1}{2}\right) \lambda$$

$\varphi_n = \arcsin \left(\frac{\left(n + \frac{1}{2}\right) \lambda}{a} \right)$ } koti, pri katerih so oslabitve

DOPLERJEV POJAV



sprejemnik

ν ... frekvenca oddajnika ($t_0 = \frac{1}{\nu}$)

λ ... valovna dolžina

c ... hitrost zvoka v snovi

ν' ... frekvenca, ki jo sliši sprejemnik

v_1 ... hitrost, s kateršno se giblje oddajnik

v_2 ... hitrost, s kateršno se giblje sprejemnik

(a) $v_1 = v_2 = 0$: $\nu' = \nu$

(b) $v_2 = 0, v_1 \neq 0$: (oddajnik se premika)

$t_1 = 0$... odda 1. valovno čelo

$t = t_0$... ct

$$\lambda = ct_0 - v_1 t_0 = (c - v_1) t_0 = \frac{c - v_1}{\nu}$$

$$\nu' = \frac{c}{\lambda} = \frac{c\nu}{c - v_1} = \frac{\nu}{1 - \frac{v_1}{c}} \quad \nu' > \nu \quad \text{se približuje}$$

$$\nu' = \nu \frac{1}{1 + \frac{v_1}{c}} \quad \nu' < \nu \quad \text{se oddaljuje}$$

(c) $v_1 = 0, v_2 \neq 0$ (sprejemnik se približuje)

$t = 0$

$t = t_0$: $v_2 t_0$ (razdalja, ki jo prepotuje sprejemnik)

$$ct_0 \Rightarrow ct_0 + v_2 t_0 = \lambda = \frac{c}{\nu} \rightarrow \frac{1}{\nu'} (c + v_2) = \frac{c}{\nu}$$

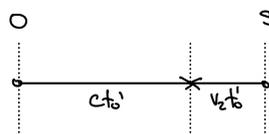
$$\Rightarrow \nu' = \nu \left(1 + \frac{v_2}{c}\right)$$

se približuje

$$\nu' = \nu \left(1 - \frac{v_2}{c}\right)$$

se oddaljuje

(d) $\nu' = \nu \frac{1 \pm \frac{v_1}{c}}{1 \pm \frac{v_2}{c}}$



2. ELEKTROSTATIKA

ELEKTRIČNA SILA, ELEKTRIČNI NABOJ, ELEKTRIČNO POLJE

$H^+ \quad H^+$
 r ← masa protona H^+
 $m_p = 1.7 \cdot 10^{-27} \text{ kg}$
 $G = 6.7 \cdot 10^{-11} \frac{\text{Nm}^2}{\text{kg}^2}$
 $r = 1 \text{ cm}$

$F_g = \frac{G m_p^2}{r^2} = 2 \cdot 10^{-60} \text{ N}$ ← izvor: m_p, m_p

Opazimo: • odbojna sila
• mnogo večja od F_g

ELEKTRIČNA SILA

sila $F_{el} = 2 \cdot 10^{-24} \text{ N}$
 $(\frac{F_{el}}{F_g} \approx 10^{36})$

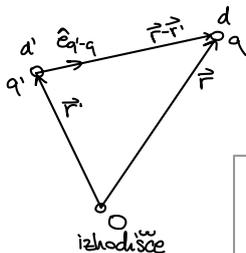
izvor: električni naboj

p, e ; F_{ee} privlačna
 q_p : naboj protona
 q_e : naboj elektrona

$|q_p| = |q_e| = q_0 = 1.602176634 \cdot 10^{-19} \text{ As}$
 OSNOVNI NABOJ

$q_p = +q_0$
 $q_e = -q_0$

Coulomb: $F_{el} \propto \frac{1}{r^2}$
 $F_{el} \propto \frac{q_1 q_2}{r^2}$



- $|\vec{r}_1 - \vec{r}_2| \Rightarrow d, d'$
- $\hat{e}_{q_1 \rightarrow q_2} = \frac{(\vec{r}_2 - \vec{r}_1)}{|\vec{r}_2 - \vec{r}_1|}$

$$\vec{F}_{q_1 \rightarrow q_2} = \frac{q_1 q_2}{4\pi\epsilon_0} \frac{\hat{e}_{q_1 \rightarrow q_2}}{|\vec{r}_2 - \vec{r}_1|^2} = \frac{q_1 q_2}{4\pi\epsilon_0} \frac{(\vec{r}_2 - \vec{r}_1)}{|\vec{r}_2 - \vec{r}_1|^3}$$

ELEKTRIČNA KONSTANTA

$\epsilon_0 = 8.85 \cdot 10^{-12} \frac{(\text{As})^2}{\text{Nm}^2} / \frac{\text{As}}{\text{Vm}}$

← COULOMBOV ZAKON

VOLT

$V = \frac{\text{Nm}}{\text{As}}$

$\Rightarrow \frac{(\text{As})^2}{\text{Nm}^2} = \frac{\text{As}}{\text{Vm}}$

$\Rightarrow N = \frac{\text{VAs}}{\text{m}}$

$q_1 q_2 \Rightarrow m_1, m_2$:

$\vec{F}_{m_1 \rightarrow m_2} = -G m_1 m_2 \frac{(\vec{r}_2 - \vec{r}_1)}{|\vec{r}_2 - \vec{r}_1|^3}$ ← gravitacijska sila med dvema masama

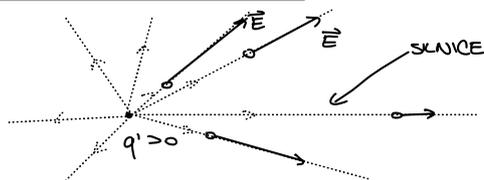
POJEM ELEKTRIČNEGA POLJA:

naboj q' : spremeni lastnosti prostora v svoji okolici
 \Rightarrow ustvari električno polje

$\vec{E}_{q'}(\vec{r}) = \frac{\vec{F}_{q' \rightarrow q}}{q}$ [$\frac{\text{N}}{\text{As}} = \frac{\text{V}}{\text{m}}$]

→ ZAKON ELEKTRIČNEGA POLJA (v točki z \vec{r} , na račun q')

$\Rightarrow \vec{E}_{q'}(\vec{r}) = \frac{q'}{4\pi\epsilon_0} \frac{(\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3}$



- $q_1'; \vec{r}_1'$
- $q_2'; \vec{r}_2'$
- ...
- $q_n'; \vec{r}_n'$

$\vec{r}, \vec{E}(\vec{r}) = ?$

$\vec{F}_{q_1' \rightarrow q} = q \vec{E}_{q_1'}$
 $\vec{F}_{q_2' \rightarrow q} = q \vec{E}_{q_2'}$
 \vdots
 $\vec{F}_{q_n' \rightarrow q} = q \vec{E}_{q_n'}$

učelo superpozicije

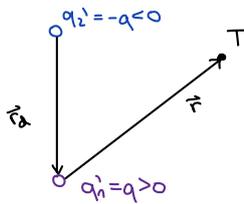
$\vec{F}_q = \sum_{i=1}^n \vec{F}_{q_i' \rightarrow q}$

$\vec{E}(\vec{r}) = \frac{\vec{F}_q}{q} \Rightarrow \vec{F}_q = q \vec{E}$

$\Rightarrow q \vec{E} = \sum_{i=1}^n q \vec{E}_{q_i'} = q \sum_{i=1}^n \vec{E}_{q_i'}$

$\Rightarrow \vec{E} = \sum_{i=1}^n \vec{E}_{q_i'}$

ELEKTRIČNO POLJE V OKOLICI ELEKTRIČNEGA DIPOLA:



$$\vec{E}(\vec{r}) = \vec{E}_{q_1}(\vec{r}) + \vec{E}_{q_2}(\vec{r})$$

Poseben primer: (T daleč stran od dipola)
 $|\vec{r}| = r \gg r_d$

$$\vec{E} \approx \frac{1}{4\pi\epsilon_0 r^3} [\partial(\vec{p}_e \cdot \hat{e}_r) \hat{e}_r - \vec{p}_e]$$

$\hat{e}_r = \frac{\vec{r}}{r}$
 $\vec{p}_e = q\vec{r}_d$
[Asm]

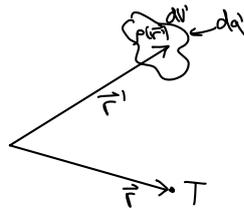
← ELEKTRIČNI DIPOLNI MOMENT

ELEKTRIČNO POLJE V OKOLICI ZVEZNO PORAZDELJENEGA NABOJA

o to je matematični model (v naravi tega ni)

$q = Nq_0, N \in \mathbb{Z}$
 prosti naboji v naravi (mnogokratniki osnovnega naboja)

$\rho(\vec{r}')$: $dq' = \rho(\vec{r}') dV'$
 ↑ GOSTOTA ELEKTRIČNEGA NABOJA
 $\rightarrow \rho(\vec{r}') = \frac{dq'}{dV'}$

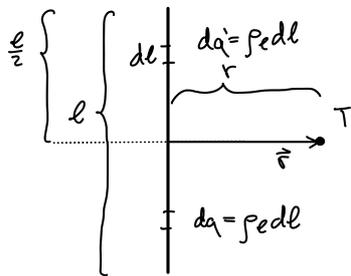


$$d\vec{E} = \frac{dq' (\vec{r} - \vec{r}')}{4\pi\epsilon_0 |\vec{r} - \vec{r}'|^3} = \frac{\rho(\vec{r}') (\vec{r} - \vec{r}')}{4\pi\epsilon_0 |\vec{r} - \vec{r}'|^3} dV'$$

$$\Rightarrow \vec{E}(\vec{r}) = \int_{\mathbb{R}^3} \frac{\rho(\vec{r}') (\vec{r} - \vec{r}')}{4\pi\epsilon_0 |\vec{r} - \vec{r}'|^3} dV'$$

PRIMERI:

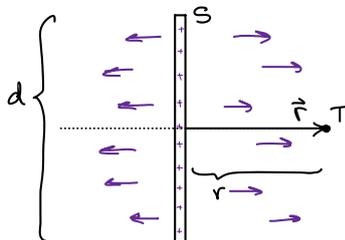
(1) \vec{E} na simetrični zelo dolge ravne enakomerno nabite žice



$\rho_l \dots$ dolžinska gostota naboja
 $\rho_l = \frac{q}{l} = \text{konst.}$

$$\vec{E}(\vec{r}) = \frac{\rho_l}{2\pi\epsilon_0 r} \hat{e}_r ; \hat{e}_r = \frac{\vec{r}}{r}$$

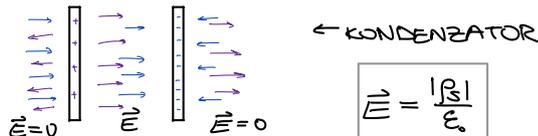
(2) \vec{E} na simetrični velike enakomerno nabite okrogle plošče



$d \gg r \quad \rho_s = \frac{q}{S} = \text{konst.}$

$$\vec{E} = \frac{\rho_s}{2\epsilon_0} \hat{e}_r \leftarrow \text{neodvisno od oddaljenosti (r)}$$

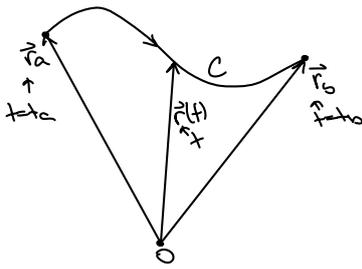
$\Rightarrow \vec{E}$ blizu plošče homogeno



\hat{e}_E : od + proti -

ELEKTRIČNA NAPETOST, ELEKTRIČNI POTENCIAL, DELO ELEKTRIČNE SILE

$$\vec{E}(\vec{r}) = \frac{1}{4\pi\epsilon_0} \int_{\mathbb{R}^3} \rho(\vec{r}') \frac{(\vec{r}-\vec{r}')}{|\vec{r}-\vec{r}'|^3} dV'$$



ELEKTRIČNA NAPETOST med \vec{r}_a in \vec{r}_b po C

$$U(\vec{r}_a \rightarrow \vec{r}_b; C) = - \int_C \vec{E} d\vec{s} \quad [V]$$

$$\Phi(\vec{r}) = \frac{1}{4\pi\epsilon_0} \int_{\mathbb{R}^3} \frac{\rho(\vec{r}')}{|\vec{r}-\vec{r}'|} dV' \quad \left[\frac{AsVm^3}{m^3Asm} = V \right]$$

ELEKTRIČNI POTENCIAL v točki \vec{r}

Zveza med \vec{E} in Φ :

$\nabla\Phi$ - predpostavimo, da ∇ in $\int_{\mathbb{R}^3} dV'$ lahko zamenjamo

$$\nabla\Phi = \frac{1}{4\pi\epsilon_0} \nabla \int_{\mathbb{R}^3} \frac{\rho(\vec{r}')}{|\vec{r}-\vec{r}'|} dV' = \frac{1}{4\pi\epsilon_0} \int_{\mathbb{R}^3} \nabla \left(\frac{\rho(\vec{r}')}{|\vec{r}-\vec{r}'|} \right) dV' = \frac{1}{4\pi\epsilon_0} \int_{\mathbb{R}^3} \rho(\vec{r}') \nabla \left(\frac{1}{|\vec{r}-\vec{r}'|} \right) dV' = -\vec{E}$$

$$\nabla \left(\frac{1}{|\vec{r}-\vec{r}'|} \right) = (\partial_x(\dots), \partial_y(\dots), \partial_z(\dots)) = (x-x'), (y-y'), (z-z') \frac{-1}{|\vec{r}-\vec{r}'|^3} = - \frac{(\vec{r}-\vec{r}')}{|\vec{r}-\vec{r}'|^3}$$

$$\partial_x(\dots) = -\frac{1}{2} [x-x']^2 + (y-y')^2 + (z-z')^2 \Big]^{-\frac{3}{2}} 2(x-x') = \frac{(x-x')}{|\vec{r}-\vec{r}'|^3}$$

(simetrično ∂_y in ∂_z)

$$\Rightarrow \vec{E} = -\nabla\Phi$$

← velja v elektrostatiskem polju, ne v splošnem

$$\Rightarrow \nabla \times \vec{E} = 0$$

← IZREK O ELEKTRIČNI NAPETOSTI V DIFERENCIALNI OBLIKI ($\nabla \times \nabla\Phi = 0$)
rotor

Posledice:

(a) $U(\vec{r}_a \rightarrow \vec{r}_b, C)$ neodvisna od C

$$\nabla\Phi \vec{r} = \dot{\Phi} = \frac{\partial\Phi}{\partial x} \dot{x} + \frac{\partial\Phi}{\partial y} \dot{y} + \frac{\partial\Phi}{\partial z} \dot{z} = \begin{bmatrix} \frac{\partial\Phi}{\partial x} \\ \frac{\partial\Phi}{\partial y} \\ \frac{\partial\Phi}{\partial z} \end{bmatrix} \cdot \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{bmatrix}$$

$$-\int_C \vec{E} d\vec{s} = -\int_{t_a}^{t_b} \vec{E} \cdot \vec{r} dt = -\int_{t_a}^{t_b} -\nabla\Phi \vec{r} dt = \int_{t_a}^{t_b} \dot{\Phi} dt = \Phi(t_b) - \Phi(t_a) = U(\vec{r}_a \rightarrow \vec{r}_b)$$

(b) $\partial S = C \dots$ zaključena pot:

$$-\oint_{\partial S} \vec{E} d\vec{s} = \Phi(\vec{r}_b) - \Phi(\vec{r}_a) = 0$$

$$\Rightarrow \oint_{\partial S} \vec{E} d\vec{s} = 0$$

← IZREK O ELEKTRIČNI NAPETOSTI V INTEGRALSKI OBLIKI

Stokesov izrek: ∂S : gladka orientabilna ploskev, E_x, E_y, E_z

$$\oint_{\partial S} \vec{E} d\vec{s} = \int_S (\nabla \times \vec{E}) d\vec{S} = \int_S \vec{0} dS = 0$$

q testni naboj v \vec{E} :

\vec{F} konservativna

$$W_{e,p} = q\Phi$$

$$A_{el} = \int_C \vec{F} d\vec{s} = \int_C q\vec{E} d\vec{s} = q \int_C \vec{E} d\vec{s} = -qU(\vec{r}_a \rightarrow \vec{r}_b) = -q[\Phi(\vec{r}_b) - \Phi(\vec{r}_a)] = -\Delta W_{e,p}$$

↑ DELO ELEKTRIČNE SILE

Primer: napetost U med ploščama kondenzatorja:

$$\vec{r}_a = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}, \oplus \text{ središče pozitivno nabite plošče} \quad \vec{r}_b = \begin{bmatrix} l \\ 0 \\ 0 \end{bmatrix}, \ominus \text{ središče negativno nabite plošče}$$

$$\vec{r} = \begin{bmatrix} x \\ y \\ z \end{bmatrix}; \quad \vec{r}' = \begin{bmatrix} x' \\ y' \\ z' \end{bmatrix}$$

$$U(\vec{r}_a \rightarrow \vec{r}_b) = - \int_C \vec{E} \cdot d\vec{s} = - \int_{t_a}^{t_b} \vec{E} \cdot \dot{\vec{r}} dt = - \int_{t_a}^{t_b} \frac{\rho}{\epsilon_0} \hat{e}_x \cdot \dot{\vec{r}} dt = - \int_{t_a}^{t_b} \frac{\rho}{\epsilon_0} \dot{x} dt = - \frac{\rho}{\epsilon_0} \int_{t_a}^{t_b} \dot{x} dt = - \frac{\rho}{\epsilon_0} (x|_{t=t_b} - x|_{t=t_a}) = - \frac{\rho l}{\epsilon_0}$$

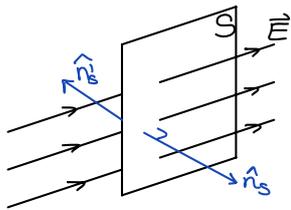
$$\Rightarrow |U| = \frac{|\rho| l}{\epsilon_0}$$

$$\rightarrow C = \frac{|\rho| l}{|U|} = \frac{\epsilon_0 S}{l} \quad [F = \frac{As}{V}]$$

KAPACITETA KONDENZATORJA

PRETOK ELEKTRIČNEGA POLJA, Φ_E (ELEKTRIČNI PRETOK)

HOMOGENO ELEKTRIČNO POLJE \vec{E} , ravna ploskev:



$$\vec{S} = S \cdot \hat{n}_s$$

Intuitivno: štejeemo silnice, ki prebadajo ploskev

$$\text{Formalno: } \Phi_E = \epsilon_0 \vec{E} \cdot \vec{S} = \epsilon_0 \vec{E} \cdot S \hat{n}_s \quad \left[\frac{As \cdot V \cdot m^{-2}}{Vm^{-1}} = As \right]$$

SPLOŠNA DEFINICIJA: Φ_E (poglej ne nujno homogeno in ravno)

$$\vec{S} \rightarrow d\vec{S} = \hat{n}_s dS \sim \text{približna ravna majhna ploskev}$$

$$d\Phi_E = \epsilon_0 \vec{E} \cdot d\vec{S}$$

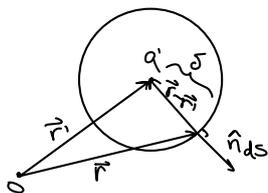
$$\Rightarrow \Phi_E = \int_S \epsilon_0 \vec{E} \cdot d\vec{S} = \epsilon_0 \int_S \vec{E} \cdot \hat{n}_s dS$$

$$\vec{E} \cdot \vec{S} = ES \cos \beta \quad \left\{ \begin{array}{l} \leftarrow \text{ES} \\ \downarrow \end{array} \right.$$

Komentar: a) Φ_E je skalar (nima smeri), ima pa predznak: $\text{sgn } \Phi_E = \begin{cases} 1; & \beta \text{ oster} \\ -1; & \beta \text{ tup} \end{cases}$

b) Predznak Φ_E odvisen od izbire \hat{n}_s ali $\hat{n}_s' = -\hat{n}_s$.

Primer: kroglja $K(\vec{r}, \sigma)$ in sfera ∂K : $S = \int_{\partial K} dS = 4\pi\sigma^2$
 \hat{n}_s zunanja normala



$$\hat{n}_s = \frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|}$$

$$\vec{E}_q(\vec{r}) = \frac{q'}{4\pi\epsilon_0} \frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3}$$

$$\left. \begin{array}{l} \hat{n}_s = \frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|} \\ \vec{E}_q(\vec{r}) = \frac{q'}{4\pi\epsilon_0} \frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3} \end{array} \right\} \Rightarrow \vec{E} \cdot d\vec{S} = \vec{E} \cdot \hat{n}_s dS = \frac{q'}{4\pi\epsilon_0} \frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3} \cdot \frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|} dS = \frac{q'}{4\pi\epsilon_0} \frac{1}{|\vec{r} - \vec{r}'|^2} dS = \frac{q'}{4\pi\epsilon_0 \sigma^2} dS$$

$$\Rightarrow \Phi_E = \frac{\epsilon_0 q'}{4\pi\epsilon_0 \sigma^2} \int_{\partial K} dS = \frac{q'}{4\pi\sigma^2} 4\pi\sigma^2 = q'$$

IZREK O ELEKTRIČNEM PRETOKU:

$$\Phi_E(\partial V) = \int_V \rho dV$$

↑ zadržati naboj
↑ zaključena ploskev

$$\int_{\partial V} \epsilon_0 \vec{E} d\vec{S} = \int_V \rho dV$$

IZREK O ELEKTRIČNEM PRETOKU
V DIFERENCIALNI OBLIKI

Gauss: $\int_{\partial V} \epsilon_0 \vec{E} d\vec{S} = \int_V \epsilon_0 \nabla \cdot \vec{E} dV = \int_V \rho dV \Rightarrow \epsilon_0 \nabla \cdot \vec{E} = \rho \Rightarrow \nabla \cdot \vec{E} = \frac{\rho}{\epsilon_0}$

REORGANIZACIJA ("obrnjena logika")

Izrek (Helmholtz): $\vec{E} \in \mathbb{R}^3, r \rightarrow \infty, \vec{E}$ vsaj $\frac{1}{r}$:

$$\Rightarrow \vec{E} = -\nabla \Phi + \nabla \times \vec{A}$$

$$\Phi = \frac{1}{4\pi} \int_{\mathbb{R}^3} \frac{\nabla' \cdot \vec{E}(\vec{r}')}{|\vec{r} - \vec{r}'|} dV' \quad (\nabla' = (\frac{\partial}{\partial x'}, \frac{\partial}{\partial y'}, \frac{\partial}{\partial z'}))$$

$$\vec{A} = \frac{1}{4\pi} \int_{\mathbb{R}^3} \frac{\nabla' \times \vec{E}(\vec{r}')}{|\vec{r} - \vec{r}'|^3} dV'$$

Električno polje \vec{E} : $\nabla \times \vec{E}(\vec{r}) = 0 \Rightarrow \nabla' \times \vec{E}(\vec{r}') = 0$

Izrek: $\nabla \cdot \vec{E} = \frac{\rho}{\epsilon_0}$

$$\Rightarrow \vec{E} = -\nabla \left[\frac{1}{4\pi} \int_{\mathbb{R}^3} \frac{\nabla' \cdot \vec{E}(\vec{r}')}{|\vec{r} - \vec{r}'|} dV' \right] + \nabla \times \vec{A}$$

$$= -\nabla \left[\frac{1}{4\pi} \int_{\mathbb{R}^3} \frac{\rho(\vec{r}')}{\epsilon_0} \frac{1}{|\vec{r} - \vec{r}'|} dV' \right] + \nabla \times \vec{A}$$

$$= -\int_{\mathbb{R}^3} \frac{\rho(\vec{r}')}{4\pi\epsilon_0} \nabla \left[\frac{1}{|\vec{r} - \vec{r}'|} \right] dV' = \int_{\mathbb{R}^3} \frac{\rho(\vec{r}')}{4\pi\epsilon_0} \frac{(\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3} dV'$$

COULOMBOV IZREK (zakon) *

(Do sedaj: Coulombov zakon $\vec{E} \stackrel{\text{def.}}{\rightarrow} \vec{F}_{q \rightarrow q} = q\vec{E}_q$ superpozicija $\vec{E}_{\rho(\vec{r})}(\vec{r}) = \int_{\mathbb{R}^3} \frac{\rho(\vec{r}')}{4\pi\epsilon_0} \frac{(\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3} dV'$... izrek $\nabla \times \vec{E} = 0$ in $\nabla \cdot \vec{E} = \frac{\rho}{\epsilon_0}$)

Sedaj: $\nabla \times \vec{E} = 0; \nabla \cdot \vec{E} = \frac{\rho}{\epsilon_0}, \vec{F} = q\vec{E} \xrightarrow{\text{izrek}} \vec{E}(\vec{r}) \dots$

FIZIKALNI ZAKONI COULOMBOV IZREK

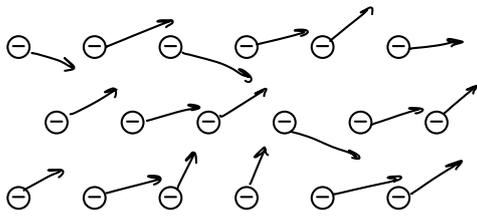
Komentar: $\nabla \cdot \vec{E} = \frac{\rho}{\epsilon_0}$ tudi velja za premikajoče naboje (izven polja)
 $\nabla \times \vec{E} = 0$ res, če nimamo spremenljivih magnetnih polj: $\frac{\partial \vec{B}}{\partial t} = 0$

Komentar: $\vec{F} = q\vec{E}$ res tudi, če $\vec{v}_q \neq 0$

3. ELEKTRIČNI TOK

Opazovali bomo gibanje nabojev pod vplivom (zunanjega) električnega polja.

GOSTOTA ELEKTRIČNEGA TOKA



število prostogibljivih nabojev

$$n \equiv \frac{N}{V} \quad \left[\frac{1}{m^3} \right]$$

q_1 [As] \Rightarrow $\rho_e \equiv q_1 n \quad \left[\frac{As}{m^3} \right]$

↑ številska gostota gibljivih nabojev

← naboj enega nosilca

$$\vec{v} = \frac{1}{N} \sum_i \vec{v}_i$$

\Rightarrow $\vec{j}_e \equiv \rho_e \vec{v}$ ← GOSTOTA ELEKTRIČNEGA TOKA $\left[\frac{A}{m^2} \right]$

$v = |\vec{v}| > 0$; $\hat{e}_v \equiv \frac{\vec{v}}{v} \Rightarrow \vec{v} = v \cdot \hat{e}_v$

\Rightarrow $\vec{j}_e = \rho_e v \hat{e}_v = q_1 n v \hat{e}_v$

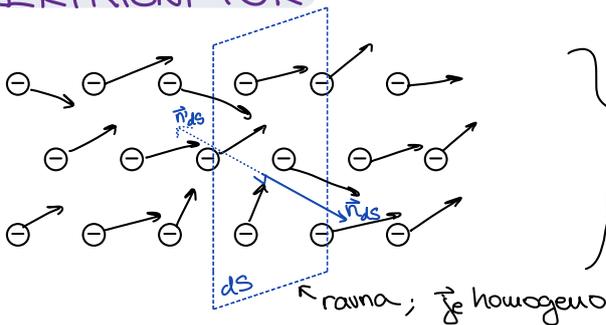
$j_e = |\vec{j}_e| > 0$, $\hat{e}_{j_e} = \frac{\vec{j}_e}{j_e} \Rightarrow \vec{j}_e = j_e \hat{e}_{j_e}$

↑ smer gostote električnega toka (smer električnega toka)

$j = |\vec{j}| = |\rho_e \vec{v}| = |\rho_e| v \Rightarrow \vec{j}_e = |\rho_e| v \hat{e}_j$

$\Rightarrow \rho_e v \hat{e}_v = |\rho_e| v \hat{e}_j \Rightarrow \hat{e}_j = \hat{e}_v \frac{\rho_e}{|\rho_e|} = \begin{cases} +\hat{e}_v; & \rho_e > 0 \\ -\hat{e}_v; & \rho_e < 0 \end{cases}$

ELEKTRIČNI TOK



ELEKTRIČNI TOK SKOZI dS

$$dI = \vec{j}_e \cdot d\vec{S} \quad [A]$$

Splošna definicija: (S ukrivljena, \vec{j}_e nehomogeno)

$$I \equiv \int dI = \int_S \vec{j}_e \cdot d\vec{S} \quad [A]$$

← pretok

Analogija: $\vec{j}_e \Leftrightarrow \epsilon_0 \vec{E}$

$$I = \int_S \vec{j}_e \cdot d\vec{S} \Leftrightarrow \Phi_E = \int_S \epsilon_0 \vec{E} \cdot d\vec{S}$$

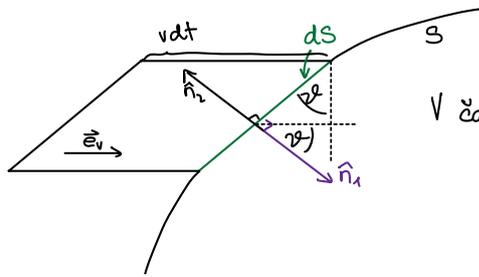
\Rightarrow I nima smeri

\Rightarrow predznak odvisen od izbire orientacije ploskve (\hat{n}_s ali $-\hat{n}_s$)

Primer: homogeno \vec{j}_e , ravna S ($\hat{n}_{ds} = \hat{n}_s$)

$$I = \int_S \vec{j}_e \cdot d\vec{S} = \int_S j_e \hat{e}_j \hat{n}_s \cdot d\vec{S} = j_e \hat{e}_j \hat{n}_s \int_S dS = j_e \hat{e}_j \hat{n}_s S = \vec{j}_e \vec{S}$$

INTERPRETACIJA ELEKTRIČNEGA TOKA



$I \equiv$ pretok (\vec{j})

V času dt : $d^3V = v dt d^2S \cos \alpha$; $\cos \alpha = \hat{e}_v \cdot \hat{n}_1$
 $= v \cdot dt \cdot d^2S \hat{e}_v \cdot \hat{n}_1$

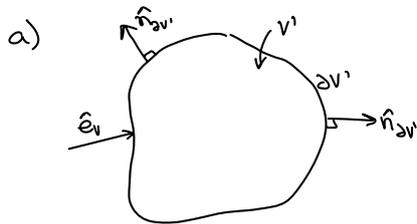
$d^3N = n \cdot d^3V = dt n v \hat{e}_v \cdot \hat{n}_1 d^2S$

$d^3q = q_n d^3N = dt q_n n v \hat{e}_v \cdot \hat{n}_1 d^2S$
 $= dt \int_{\hat{n}_1} \vec{j}_e \cdot \hat{n}_1 d^2S$
 $= dt \int_{\hat{n}_1} \vec{j}_e \cdot d^2\vec{S}_n$

$\Rightarrow dq = dt \int_{\hat{n}_1} \vec{j}_e \cdot d^2\vec{S}_n \Rightarrow I_{\hat{n}_1} = \frac{dq}{dt}$; $\hat{n}_1 \hat{e}_v > 0$
 $I_{\hat{n}_2} = -\frac{dq}{dt}$; $\hat{n}_2 \hat{e}_v < 0$

$\Rightarrow dq = \begin{cases} I dt; & \hat{n} \hat{e}_v > 0 \\ -I dt; & \hat{n} \hat{e}_v < 0 \end{cases}$

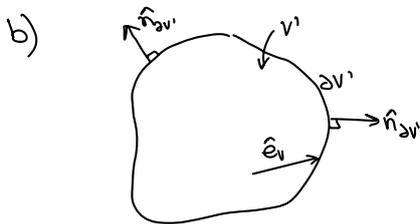
ZAKON O OHRANITVI ELEKTRIČNEGA NABOJA, KONTINUITETNA ENAČBA in PRVI KIRCHOFFOV IZREK



\hat{e}_v v V' (naboji pritekaajo v V')
 $\Rightarrow \hat{e}_v \cdot \hat{n}_{\partial V'} < 0 \Rightarrow dq = -I dt$

$dq'_{\partial V'}$... sprememba naboja v V' zaradi pretakanja skozi $\partial V'$

$dq'_{\partial V'} = dq = -I dt$



\hat{e}_v iz V' (naboji tečejo iz V')
 $\Rightarrow \hat{e}_v \cdot \hat{n}_{\partial V'} > 0 \Rightarrow dq = I dt$

$\Rightarrow dq'_{\partial V'} = -dq = -I dt$

V splošnem: $dq'_{\partial V'} = -dt \oint_{\partial V'} \vec{j}_e \cdot d\vec{S} = -dt \iiint_V \nabla \cdot \vec{j} dV$

q' : celoten naboj v V'

$q' = \iiint_{V'} \rho_e dV$

$\frac{\partial q'}{\partial t}$: sprememba naboja v (fiksni) V' na enoto časa

$\frac{\partial q'}{\partial t} = \frac{\partial}{\partial t} \iiint_{V'} \rho_e(\vec{r}) dV = \iiint_{V'} \frac{\partial \rho_e}{\partial t} dV$

dq' : sprememba naboja v V' v intervalu dt

$dq' = \frac{\partial q'}{\partial t} dt = dt \iiint_{V'} \frac{\partial \rho_e}{\partial t} dV$

ZAKON O OHRANITVI ELEKTRIČNEGA NABOJA (fizikalni zakon, eksperimentalno dejstvo)

naboja ne moremo ne ustvariti ne izničiti

$dq' = dq'_{\partial V'}$

$$\Rightarrow dt \iiint_V \frac{\partial \rho}{\partial t} dV = -dt \iiint_V \nabla \cdot \vec{j} dV$$

$$dt \iiint_V \frac{\partial \rho}{\partial t} dV = \iiint_V -\nabla \cdot \vec{j} dV \Rightarrow \iiint_V \left(\frac{\partial \rho}{\partial t} + \nabla \cdot \vec{j} \right) dV = 0, \forall V'$$

$$\Rightarrow \boxed{\frac{\partial \rho}{\partial t} = -\nabla \cdot \vec{j}} \leftarrow \text{KONTINUITETNA ENAČBA}$$

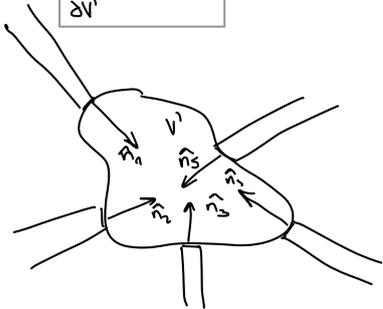
(diferencialna oblika)

$$\iiint_V \frac{\partial \rho}{\partial t} dV = \oint_{\partial V'} \vec{j} \cdot d\vec{S} = \frac{\partial q'}{\partial t} \quad (\text{integralna oblika})$$

Poseben primer: $\frac{\partial \rho}{\partial t} = 0$

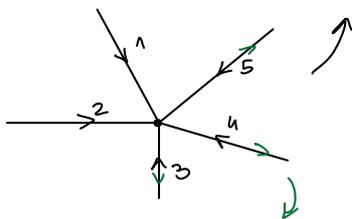
$$\Rightarrow \nabla \cdot \vec{j} = 0 \Rightarrow \iiint_V \nabla \cdot \vec{j} = 0 \Rightarrow \oint_{\partial V'} \vec{j} \cdot d\vec{S} = 0$$

$$\Rightarrow \oint_{\partial V'} \vec{j} \cdot d\vec{S} = 0; \hat{n}_{\partial V'} \text{ vsi kažejo v isto smer; npr. v } V'$$



$$I_i = \int_{\partial V'_i} \vec{j} \cdot d\vec{S}$$

$$\oint_{\partial V'} \vec{j} \cdot d\vec{S} = \sum_{i=1}^5 \int_{\partial V'_i} \vec{j} \cdot d\vec{S} = \sum_{i=1}^5 I_i$$



$$\sum_i I_i = 0 \leftarrow \text{1. KIRCHOFFOV IZREK}$$

$$I_3' = -I_3, I_4' = -I_4, I_5' = -I_5 : \sum_1^5 I_i = \sum_1^2 I_i - \sum_3^5 I_i = \sum_1^2 I_i - \sum_1^3 I_i' = 0$$

$$\Rightarrow \sum_1^2 I_i = \sum_1^3 I_i'$$

OHMOV ZAKON

$$\vec{j} = \frac{1}{\xi} \vec{E}$$

ξ : specifična upornost snovi (pravilna oznaka ξ)
 $\left[\frac{V}{m} \frac{m^2}{A} = \frac{Vm}{A} = \Omega m = \Omega \frac{mm^2}{m} \right]$

$$\vec{j} \propto \vec{E}$$

material	$\xi \left[\frac{\Omega mm^2}{m} \right]$
Cu	0,0172
Fe	0,1
slana voda	$8 \cdot 10^4$
voda	$3 \cdot 10^7$
steklo	10^{16}
SiO ₂	10^{23}

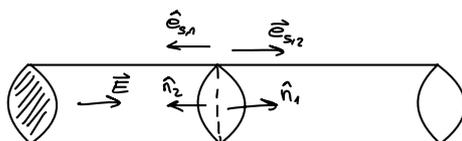
↑ PREVOĐNIKI
↓ IZOLATORJI

◦ linearni zakon upora: Drude

MAKROSKOPSKA SLIKA:

$$U, I, \xi \rightarrow R$$

zanima nas povezava



$\xi = \text{konst.}$

$$\vec{j} = \frac{1}{\xi} \vec{E} \rightarrow \vec{E} = \xi \vec{j}$$

$$\hat{n}_1 \text{ ali } \hat{n}_2 : I_{1,2} = \int \vec{j} \cdot \hat{n}_{1,2} S$$

$$\vec{e}_{s,1} \text{ ali } \vec{e}_{s,2} : U_{1,2} = - \int \vec{E} \cdot d\vec{S}_{1,2} = -\vec{E} \cdot \vec{e}_{s,1,2} l$$

(a) $\hat{e}_s = +\hat{n}$ ($\hat{e}_s = \hat{e}_{s1}$ in $\hat{n} = \hat{n}_1$ ali $\hat{e}_s = \hat{e}_{s2}$ in $\hat{n} = \hat{n}_2$)

$U = -\vec{E} \cdot \hat{e}_s l = -\vec{E} \cdot \hat{n} = -\xi \int \hat{n} l = -\frac{\xi}{\epsilon_0} l I = -RI$; $R = \frac{\xi l}{\epsilon_0 S} [\Omega]$

(b) $\hat{e}_s = -\hat{n}$
 $\Rightarrow U = -\vec{E} \cdot \hat{e}_s l = -\vec{E} \cdot (-\hat{n}) l = \vec{E} \cdot \hat{n} l = \xi \int \hat{n} l = \xi l \frac{I}{\epsilon_0 S} = RI$

$|I| = jS = n v q_0 S$; $n = \frac{N}{V} = \frac{1}{V} \frac{m}{M} N_A = \frac{\rho N_A}{M}$
↑ avoquadro številka

Primer:

baker (Cu): $S = 1 \text{ mm}^2 = 10^{-6} \text{ m}^2$

$I = 1 \text{ A}$

$\rho_{Cu} = 9 \cdot 10^3 \frac{\text{kg}}{\text{m}^3}$

$M_{Cu} = 63,5 \frac{\text{kg}}{\text{kmol}}$

$N_A = 6 \cdot 10^{26} \text{ kmol}^{-1}$

$v = ?$

$v = \frac{|I|}{n S q_0} = \frac{|I| \cdot M_{Cu}}{\rho_{Cu} \cdot N_A \cdot S q_0} =$

$= \frac{1 \text{ A} \cdot 63,5 \text{ kg m}^3 \text{ kmol}^{-1}}{\text{kmol} \cdot 9 \cdot 10^3 \text{ kg} \cdot 6 \cdot 10^{26} \cdot 10^{-6} \text{ m}^2 \cdot 1,6 \cdot 10^{-19} \text{ As}} =$

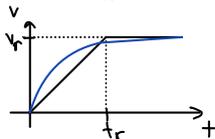
$= \frac{63,5}{9 \cdot 6 \cdot 1,6} \cdot 10^{-4} \frac{\text{m}}{\text{s}} \approx 0,1 \frac{\text{mm}}{\text{s}}$

Primer:

Cu, $v = 0 \rightarrow v_r = 0,1 \frac{\text{mm}}{\text{s}}$
 $t_r = ?$

$v_r = \frac{|I| \cdot M_{Cu}}{\rho_{Cu} N_A S q_0} = \frac{|I| \cdot M_{Cu}}{R \rho_{Cu} N_A S q_0} = \frac{|I| \cdot S \cdot M_{Cu}}{\xi l \rho_{Cu} N_A S q_0}$

Benostavitev: $a = \text{konst.}$



$v_r = a t_r \Rightarrow t_r = \frac{v_r}{a}$

$a = \frac{F_{el}}{m_1} = \frac{q_0 E}{m_1} = \frac{q_0 |U|}{m_1 l} = \frac{q_0 |U| N_A}{l M_{Cu} r} \quad (m_1 = \frac{m_e}{m_n} r)$

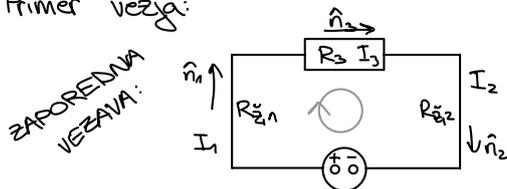
$\Rightarrow t_r = \frac{|U| M_{Cu}^2 l r}{\xi l \rho_{Cu} N_A q_0^2 |U| N_A} = \frac{M_{Cu}^2 r}{\xi \rho_{Cu} N_A^2 q_0^2} \sim \text{ps (piko sekunda)}$

DRUGI KIRCHHOFFOV ZAKON

- zakon o električni napetosti:
- omejena veljavnost: $\frac{\partial \vec{E}}{\partial t} = 0$

$$-\oint_C \vec{E} d\vec{S} = 0$$

Primer vezja:



- izberemo: a) smer dakhoda \hat{e}_s } $\hat{e}_{s,i} = \hat{n}_i$
 b) smeri $\hat{n}_1, \hat{n}_2, \hat{n}_3$ } (v našem primeru)

$$-\oint_C \vec{E} d\vec{S} = -\int_{C_1} \vec{E} d\vec{S} - \int_{C_3} \vec{E} d\vec{S} - \int_{C_2} \vec{E} d\vec{S} - \int_{C_g} \vec{E} d\vec{S} = 0$$

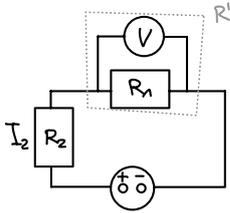
$$-\int_{C_g} \vec{E} d\vec{S} = U_g \quad \left\{ \begin{array}{l} > 0: - \rightarrow + \\ < 0: + \rightarrow - \end{array} \right. \quad (\text{naša pot: } - \rightarrow +)$$

$$-\int_{C_1} \vec{E} d\vec{S} = U_{z1} = -I R_1 \quad -\int_{C_2} \vec{E} d\vec{S} = U_{z2} = -I R_2 \quad (\text{"ker sta } \hat{e}_{n2} \text{ in } \hat{n}_{n2} \text{ v isti smeri)}$$

$$-\int_{C_3} \vec{E} d\vec{S} = U_{R3} = -I R_3$$

1. Kirchhoffov izrek $\Rightarrow I_1 = I_2 = I_3 = I$; $U_{z1} + U_{z2} + U_{R3} + U_g = 0 \Rightarrow \sum_i U_i = 0$

(b)



⊙ in R_1 vezana vzporedno

$$\frac{1}{R'} = \frac{1}{R_1} + \frac{1}{R_V} \rightarrow R' = \frac{R_1 R_V}{R_1 + R_V}$$

$$R = R_2 + R' = R_2 + \frac{R_1 R_V}{R_1 + R_V} \quad I_2 = \frac{|U_{g1}|}{R}$$

↑
zaporedno vezano

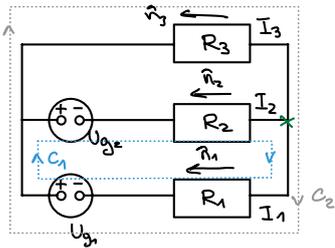
$\neq U_{R_1}$

2. Kirchhoffov izrek: $|U_{g1}| - I_2 R_2 - \underbrace{I_2 R'}_{U_V} = 0 \Rightarrow U_V = I_2 R_2 - |U_{g1}| = \frac{|U_{g1}|}{R} R_2 - |U_{g1}| = |U_{g1}| \left(\frac{R_2}{R} - 1 \right)$

$$R_V \gg R_1: R' = \frac{R_1 R_V}{R_1 + R_V} = \frac{R_1 R_V}{R_V \left(1 + \frac{R_1}{R_V} \right)} = R_1 \left(1 - \frac{R_1}{R_V} \right) \sim R_1 \Rightarrow R = R_2 + R' \approx R_2 + R_1$$

$$\Rightarrow U_V = -|U_{g1}| \left(1 - \frac{R_2}{R_1 + R_2} \right) = -|U_{g1}| \frac{R_1}{R_1 + R_2} = U_{R_1}$$

Primer:



$|U_{g1}|, |U_{g2}|, R_1, R_2, R_3; R_2 \ll R_1, R_3$

$$C_1: |U_{g1}| - |U_{g2}| + I_2 R_2 - I_1 R_1 = 0$$

$$C_2: |U_{g1}| + I_3 R_3 - I_1 R_1 = 0$$

$$\begin{cases} I_1 + I_2 + I_3 = 0 \\ \cdot R_1 \end{cases} \rightarrow R_1 I_1 + R_1 I_2 + R_1 I_3 = 0$$

↑ 1. Kirchhoffov izrek

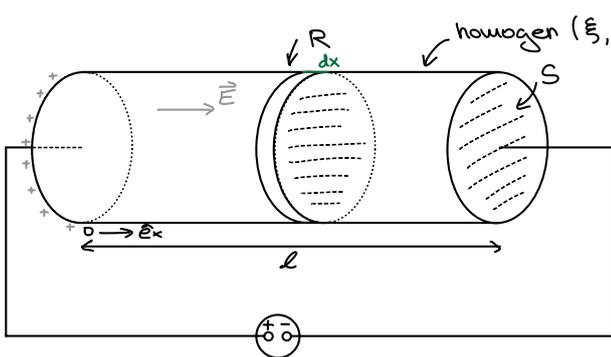
$$\begin{aligned} \rightarrow R_1 I_1 - R_2 I_2 &= |U_{g1}| - |U_{g2}| \\ R_1 I_1 - R_3 I_3 &= |U_{g1}| \\ R_1 I_1 + R_1 I_2 + R_1 I_3 &= 0 \end{aligned}$$

$$\rightarrow R = \begin{bmatrix} R_1 & -R_2 & 0 \\ R_1 & 0 & -R_3 \\ R_1 & R_1 & R_1 \end{bmatrix}; \vec{I} = \begin{bmatrix} I_1 \\ I_2 \\ I_3 \end{bmatrix}; \vec{U} = \begin{bmatrix} |U_{g1}| - |U_{g2}| \\ |U_{g1}| \\ 0 \end{bmatrix}$$

$$R \vec{I} = \vec{U}; \vec{I} = ?$$

$$\exists R^{-1} \Rightarrow \vec{I} = R^{-1} \vec{U}; R^{-1} = ? \text{ (DN)}$$

ELEKTRIČNO DELO IN ELEKTRIČNA MOČ



$$\vec{E} \text{ homogeno} \Rightarrow \vec{F}_{el} = q_1 \vec{E}$$

- $dV = S dx$
- $dl = v dt = d\vec{s}$
- $dq = \rho dV = \rho S dx$
- $d\vec{F}_{el} = dq \vec{E} = \rho S \vec{E} dx$
- $d^2 A_{el} = d\vec{F}_{el} d\vec{s} = \rho S \vec{E} v dt dx = S \vec{j} \vec{E} dt dx$

$$\text{Ohmov zakon: } \vec{j} = \frac{1}{\epsilon} \vec{E} \Rightarrow \vec{E} = \vec{j} \epsilon \Rightarrow d^2 A_{el} = S \epsilon \vec{j} \cdot \vec{j} dt dx = \overset{S \epsilon}{I_R} \cdot \frac{I_R}{S} \epsilon dt dx = \frac{\epsilon}{S} I_R^2 dx dt$$

$$\Rightarrow dA_{el} = dt \int_0^l \frac{\epsilon}{S} I_R^2 dx = dt \frac{\epsilon l}{S} I_R^2 = dt R I_R^2$$

$$\Rightarrow P_{el} = \frac{dA_{el}}{dt} = R I_R^2 \quad (>0) \quad (\vec{v} \parallel \vec{F}_{el})$$

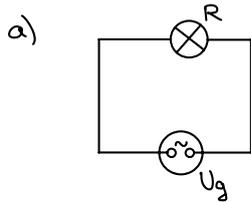
$$U_R = \pm I_R R \rightarrow I_R = \pm \frac{U_R}{R} \Rightarrow P_{el} = R \frac{U_R^2}{R^2} = \frac{U_R^2}{R}$$

Primer: $I_R \cdot U_R = \text{konst.}$

$$A_{el} = \int_0^t P_{el}(\tau) d\tau = R I_R^2 t = \frac{U_R^2}{R} t \quad P_{el} \propto A_{el}$$

ENERGIJSKI ZAKON: $A_{el} + Q_{\text{iz}} = \Delta W_n \rightarrow A_{el} \approx \Delta W_n \sim m c_p \Delta T \rightarrow P_{el} \propto \Delta T$ (sevanje)

Poskus z izmeničnim tokom: $U_g = U_0 \sin(2\pi \nu t)$; $\frac{U_0}{\sqrt{2}} = 220 \text{ V}$
 $\vec{E} = \vec{E}(t): \oint \vec{E} d\vec{s} = 0$ predpostavimo, da velja



$$U_g = U_0 \sin(\omega t); \quad \omega = 2\pi \nu = \frac{2\pi}{T_0}$$

$$U_R + U_g = 0 \Rightarrow U_R = -U_g = -U_0 \sin(\omega t)$$

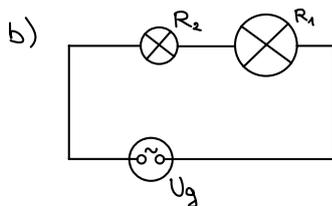
$$I_R = \pm \frac{U_R}{R} = \mp \frac{U_0}{R} \sin(\omega t) = \mp I_0 \sin(\omega t)$$

$$P_{el} = \frac{U_R^2}{R} = \frac{U_0^2}{R} \sin^2(\omega t)$$

$$A_{el} = \int_0^{t=nt_0} P_{el}(\tau) d\tau = \frac{U_0^2}{R} \int_0^{t=nt_0} \sin^2\left(\frac{2\pi}{T_0} \tau\right) d\tau = \frac{U_0^2}{R} \frac{t}{2} = \frac{U_0^2}{2R} t$$

$$A_{el} = \bar{P}_{el} \cdot t; \quad \Rightarrow \boxed{\bar{P}_{el} = \frac{1}{R} \frac{U_0^2}{2} = \frac{1}{R} \left(\frac{U_0}{\sqrt{2}}\right)^2} \quad R = \left(\frac{U_0}{\sqrt{2}}\right)^2 \frac{1}{\bar{P}_{el}}$$

Podatek na žarnici: $\frac{U_0}{\sqrt{2}} = 230 \text{ V} \Rightarrow \bar{P}_{el} = 25 \text{ W}$ $\rightarrow R \propto \frac{1}{\bar{P}_{nom}}$
 ↑ nominalna moč



$$(R_1 < R_2)$$

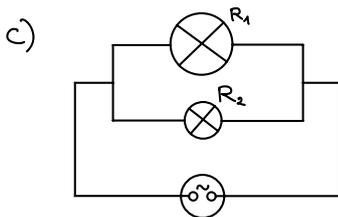
$$R = R_1 + R_2$$

$$I = \frac{U_g}{R} \Rightarrow U_{R_1} = I R_1 = \frac{U_g}{R} R_1 = U_0 \frac{R_1}{R} \sin(\omega t)$$

$$U_{R_2} = U_0 \frac{R_2}{R} \sin(\omega t)$$

$$\boxed{\bar{P}_1 = \frac{1}{2R_1} \left(\frac{U_0 R_1}{R}\right)^2 = \frac{1}{2R_1} \frac{U_0^2 R_1^2}{R^2} = \frac{U_0^2}{2R^2} R_1} \quad \text{in} \quad \boxed{\bar{P}_2 = \frac{U_0^2}{2R^2} R_2}$$

$$R = R_1 + R_2 = R_2 \left(1 + \frac{R_1}{R_2}\right) \rightarrow R^2 = R_2^2 \left(1 + \frac{R_1}{R_2}\right)^2 \approx R_2^2 \Rightarrow \bar{P}_1 \approx \frac{U_0^2}{2R_2^2} \frac{R_1^2}{R_2^2}, \quad \bar{P}_2 \approx \frac{U_0^2}{2R_2^2}$$



$$U_{R_1} = -U_g = -U_0 \sin(\omega t)$$

$$U_{R_2} = -U_0 \sin(\omega t)$$

$$\boxed{\bar{P}_1 = \frac{U_0^2}{2R_1}} \quad \boxed{\bar{P}_2 = \frac{U_0^2}{2R_2}}$$

↑ svetli močnejše

4. MAGNETNO POLJE

MAGNETNA SILA in GOSTOTA MAGNETNEGA POLJA

$$\vec{F}_e = q\vec{E}_e; \quad \vec{F}_e \neq \vec{F}_e(\vec{v}_q)$$

$$\left. \begin{array}{l} S: \vec{v}_q = 0; \quad \vec{F} = \vec{F}_e = q\vec{E}_e \neq \vec{F}(\vec{v}_q) \\ S': \vec{v}_0, \vec{v}_q = -\vec{v}_0 \Rightarrow \vec{F}' = \vec{F} \end{array} \right\} \text{Galilejeve transformacije}$$

Poskus: dva vzporedna vodnika, oba neutralna:

1. vodnik: naboj - izvori polja
2. vodnik: naboj - testni

(a) $\vec{v}_q = \vec{0}, \vec{v}_z = \vec{0}, \vec{F}_e = \vec{0}$

(b) $\vec{v}_z = \vec{0}, \vec{v}_q \neq \vec{0}, \vec{F}_e = \vec{0}$

(c) $\vec{v}_q \neq \vec{0}; \vec{v}_z = \vec{0}; \vec{F} = \vec{0}$

(d) $\vec{v}_q \neq \vec{0}, \vec{v}_z \neq \vec{0}; \vec{F} \neq \vec{0} \quad \vec{F} = \vec{F}(\vec{v}_z)$

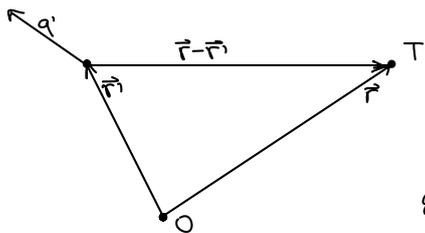
→ MAGNETNA SILA: \vec{F}_m ; $\vec{F}_m \perp \vec{v}_q$

$$\vec{F}_m = q\vec{v}_q \times \vec{B} \quad (\text{fizikalni zakon})$$

$$N = \frac{Nm}{m} = \frac{J}{m} = \frac{VAs}{m}$$

↑ GOSTOTA MAGNETNEGA POLJA $\left[\frac{VAs \cdot s}{mAsm} = \frac{Vs}{m^2} = T \right]$ ↑ TESLA

\vec{B} točkastega naboja q' , ki se giblje s konstantno hitrostjo \vec{v}_q'
(Biot-Savart-ov zakon za točkast naboj)



KONSTANTA MAGNETNEGA POLJA

$$\vec{B}(\vec{r}) = \frac{\mu_0 q'}{4\pi} \vec{v}_q' \times \frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3}$$

$$\mu_0 = 4\pi \cdot 10^{-7} \frac{Vs}{Am} \quad \left[\frac{s^2}{m^2} \right]$$

$$\epsilon_0 = 8.9 \cdot 10^{-12} \frac{As}{Vm} \Rightarrow C_0 = \frac{1}{\sqrt{\mu_0 \epsilon_0}} = 3 \cdot 10^8 \frac{m}{s}$$

$$\vec{B}(\vec{r}) = \frac{\mu_0 q'}{4\pi \epsilon_0} \vec{v}_q' \times \frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3} = \frac{1}{C_0^2} \vec{v}_q' \times \frac{q'}{4\pi \epsilon_0} \frac{(\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3} = \frac{1}{C_0^2} \vec{v}_q' \times \vec{E}(\vec{r}) = \vec{\beta}_{q'} \times \frac{\vec{E}(\vec{r})}{C_0}$$

↑ $\frac{\vec{v}_q'}{C_0}$ brez dimenzije

\vec{B} v primeru električnega toka (porazdeljenih nabojev):

$$\vec{B}(\vec{r}) = \frac{\mu_0 q'}{4\pi} \vec{v}_q' \times \frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3} \quad \rho(\vec{r}') \Rightarrow dq' = \rho(\vec{r}') dV'$$

$$\rightarrow d\vec{B}(\vec{r}) = \frac{\mu_0}{4\pi} \rho(\vec{r}') \cdot \vec{v}_q' \times \frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3} dV'$$

$$\vec{B}(\vec{r}) = \int_{\mathbb{R}^3} \frac{\mu_0}{4\pi} \rho(\vec{r}') \times \frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3} dV' \quad \rightarrow \text{náčelo superpozicije}$$

MAGNETNI (VEKTORSKI) POTENCIAL

• $\vec{E} \leftrightarrow \Phi$; $\vec{E} = -\nabla\Phi$
 ↑ skalarni potencial

• $\vec{B} \leftrightarrow \vec{A}$ ← vektorski potencial

$$\vec{A} = \frac{\mu_0}{4\pi} \int_{\mathbb{R}^3} \frac{\vec{j}(\vec{r}')}{|\vec{r}-\vec{r}'|} dV' \quad \left[\frac{\text{Vs}}{\text{Am}} \cdot \frac{\text{A}}{\text{m}^2} \cdot \frac{1}{\text{m}} \cdot \text{m}^3 = \frac{\text{Vs}}{\text{m}} = \frac{\text{Vs}}{\text{m} \cdot \text{s}} \cdot \text{m} = \text{Tm} \right]$$

⇒ $\vec{B} = \nabla \times \vec{A}$

$$\begin{aligned} \nabla \times \vec{A} &= \nabla \times \frac{\mu_0}{4\pi} \int_{\mathbb{R}^3} \frac{\vec{j}(\vec{r}')}{|\vec{r}-\vec{r}'|} dV' = \frac{\mu_0}{4\pi} \int_{\mathbb{R}^3} \nabla \times \frac{\vec{j}(\vec{r}')}{|\vec{r}-\vec{r}'|} dV' \\ &= \frac{\mu_0}{4\pi} \int_{\mathbb{R}^3} \underbrace{\left[\nabla \times \frac{1}{|\vec{r}-\vec{r}'|} \right]}_{\substack{\text{neodvisno od } x, y, z \\ \text{in } \vec{r}'}} \vec{j}(\vec{r}') - \underbrace{\vec{j}(\vec{r}') \times \nabla}_{=0} \frac{1}{|\vec{r}-\vec{r}'|} dV' \\ &= \frac{\mu_0}{4\pi} \int_{\mathbb{R}^3} \vec{j}(\vec{r}') \times \frac{\vec{r}-\vec{r}'}{|\vec{r}-\vec{r}'|^3} dV' = \vec{B} \end{aligned}$$

IZREK O MAGNETNEM PRETOKU

ploskev S : $\int_S \vec{B} d\vec{S}$ ← PRETOK MAGNETNEGA POLJA
 [Vs]

($\epsilon_0 \int_S \vec{E} d\vec{S}$ [As] pretok električnega polja)

∂V ... meja območja V (zaključena ploskev)

$\oint_{\partial V} \vec{B} d\vec{S} = 0$ ← IZREK O MAGNETNEM PRETOKU (integralska oblika) (diferencialna oblika)

$\int_{\partial V} \vec{B} d\vec{S} = \int_V \nabla \cdot \vec{B} dV = \int_V \underbrace{\nabla \cdot (\nabla \times \vec{A})}_{=0} dV = 0$ $\vec{B} = \nabla \times \vec{A} \Rightarrow \nabla \cdot \vec{B} = 0$

Primer: $\nabla \cdot \vec{E} = \frac{\rho}{\epsilon_0}$

$\oint_{\partial V} \vec{E} d\vec{S} = \frac{q}{\epsilon_0} \neq 0$

"silnice" \vec{B} → gostotnice

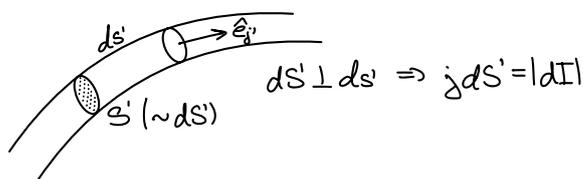
BIOT-SAVARTOV ZAKON ZA TANKE ŽICE

$\vec{A} = \frac{\mu_0}{4\pi} \int_{\mathbb{R}^3} \frac{\vec{j}(\vec{r}')}{|\vec{r}-\vec{r}'|} dV'$; $\vec{j}(\vec{r}') = j(\vec{r}') \hat{e}_j$
 $dV = dS' ds'$

$= \frac{\mu_0}{4\pi} \int_{\mathbb{R}^3} \frac{j(\vec{r}') \hat{e}_j}{|\vec{r}-\vec{r}'|} dS' ds' =$

$= \frac{\mu_0}{4\pi} \int_C \frac{\hat{e}_j ds'}{|\vec{r}-\vec{r}'|} \int_{S'} j(\vec{r}') dS' =$

$= \frac{\mu_0 |I|}{4\pi} \int_C \frac{d\vec{s}}{|\vec{r}-\vec{r}'|}$; $d\vec{s} = ds \cdot \hat{e}_j$



$$\vec{B} = \nabla \times \vec{A} =$$

$$= \nabla \times \frac{\mu_0 I I}{4\pi} \int_C \frac{d\vec{s}'}{|\vec{r}-\vec{r}'|} =$$

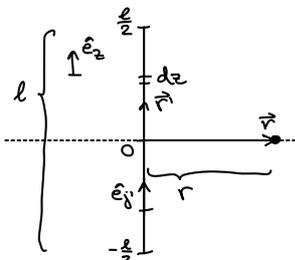
$$= \frac{\mu_0 I I}{4\pi} \int_C \nabla \times \frac{\vec{e}_j}{|\vec{r}-\vec{r}'|} ds' =$$

$$\nabla \times \frac{\vec{e}_j}{|\vec{r}-\vec{r}'|} = (\nabla \times \vec{e}_j) \frac{1}{|\vec{r}-\vec{r}'|} + \nabla \left(\frac{1}{|\vec{r}-\vec{r}'|} \right) \times \vec{e}_j = -\vec{e}_j \times \nabla \frac{1}{|\vec{r}-\vec{r}'|} = -\vec{e}_j \times \frac{(\vec{r}-\vec{r}')}{|\vec{r}-\vec{r}'|^3}$$

$$\vec{B} = \frac{\mu_0 I I}{4\pi} \int_C d\vec{s}' \times \frac{(\vec{r}-\vec{r}')}{|\vec{r}-\vec{r}'|^3}$$

← BIOT-SAVARTOV ZAKON v "originalni dolžici"

Primer: \vec{B} na simetrični dolgega ravnega vodnika s tokom:



Cilindrične koordinate: $\vec{r} = x\vec{e}_x + y\vec{e}_y + z\vec{e}_z$

$$1 = \hat{e}_\eta \cdot \hat{e}_\eta = \hat{e}_\varphi \cdot \hat{e}_\varphi = \hat{e}_z \cdot \hat{e}_z$$

$$\hat{e}_\eta \cdot \hat{e}_\varphi = \hat{e}_\varphi \cdot \hat{e}_z = \hat{e}_z \cdot \hat{e}_\eta = 0$$

$$\hat{e}_\varphi \times \hat{e}_z = \hat{e}_\eta$$

$$\hat{e}_\eta \times \hat{e}_\varphi = \hat{e}_z$$

$$\hat{e}_\eta = \varphi \hat{e}_\varphi \quad (\varphi = \varphi \hat{e}_x, \hat{e}_y)$$

$$\vec{r} = \eta \hat{e}_\eta + \varphi \hat{e}_\varphi + z \hat{e}_z$$

$$\begin{bmatrix} \cos \varphi \\ \sin \varphi \\ 0 \end{bmatrix} \quad \begin{bmatrix} -\sin \varphi \\ \cos \varphi \\ 0 \end{bmatrix}$$

$$\Rightarrow |\vec{r}-\vec{r}'|^3 = (|\vec{r}-\vec{r}'|^2)^{\frac{3}{2}} = (r^2 + z'^2)^{\frac{3}{2}}$$

$$|\vec{r}-\vec{r}'|^2 = (\vec{r}-\vec{r}') \cdot (\vec{r}-\vec{r}') = (r\hat{e}_\eta - z'\hat{e}_z) \cdot (r\hat{e}_\eta + z'\hat{e}_z) = r^2 + z'^2$$

$$\Rightarrow \vec{r} = \eta \hat{e}_\eta + z \hat{e}_z = r \hat{e}_\eta$$

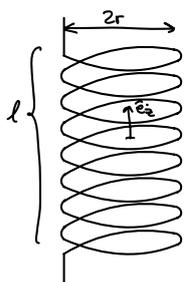
$$\vec{r}' = z' \hat{e}_z$$

$$d\vec{s}' = dz' \hat{e}_z$$

$$\begin{aligned} \Rightarrow d\vec{s}' \times (\vec{r}-\vec{r}') &= dz' \hat{e}_z \times (r\hat{e}_\eta - z'\hat{e}_z) = \\ &= dz' \hat{e}_z \times r\hat{e}_\eta = \\ &= dz' r (\hat{e}_z \times \hat{e}_\eta) = \\ &= dz' r \hat{e}_\varphi \end{aligned}$$

$$\Rightarrow \vec{B} = \frac{\mu_0 I I}{4\pi} \int_{-\frac{l}{2}}^{\frac{l}{2}} \frac{r \hat{e}_\varphi dz'}{(r^2 + z'^2)^{\frac{3}{2}}} = \frac{\mu_0 I I}{4\pi} r \hat{e}_\varphi \int_{-\frac{l}{2}}^{\frac{l}{2}} \frac{dz'}{(r^2 + z'^2)^{\frac{3}{2}}} = \frac{\mu_0 I I}{4\pi} r \hat{e}_\varphi \cdot \frac{l}{r^2} \frac{1}{(r^2 + (\frac{l}{2})^2)^{\frac{3}{2}}} \approx \frac{\mu_0 I I}{4\pi} \frac{r \hat{e}_\varphi \cdot 2}{r^2} = \frac{\mu_0 I I}{2\pi r} \hat{e}_\varphi$$

Primer: \vec{B} v tuljavi s tokom



N... število navojev

l... dolžina tuljave

I, \hat{e}_z

$2r \ll l$

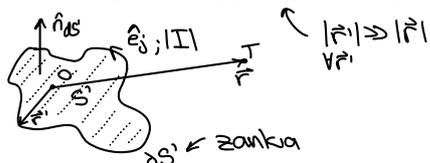
gosto navita: $\frac{N}{l}$

$$\vec{B} = \mu_0 \frac{N}{l} I I \hat{e}_B ; \hat{e}_B = \begin{cases} +\hat{e}_z ; \hat{e}_j = \hat{e}_\varphi \\ -\hat{e}_z ; \hat{e}_j = -\hat{e}_\varphi \end{cases}$$

$$\vec{B} = \mu_0 \frac{N}{l} I I \hat{e}_z (\hat{e}_j \cdot \hat{e}_\varphi) \leftarrow \text{velja znotraj tuljave}$$

$\vec{B} \approx 0$ izven tuljave (zanemljivo majhno v primerjavi s tistim skozi tuljavo)

Primer: \vec{B} v okolici drobne zanke s tokom

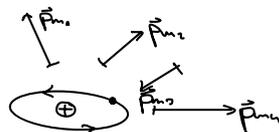


$$\vec{B}(\vec{r}) = \frac{\mu_0}{4\pi r^3} [3\hat{e}_r (\vec{p}_m \cdot \hat{e}_r) - \vec{p}_m] \leftarrow \text{MAGNETNI DIPOLNI MOMENT}$$

$$\vec{p}_m = I I S = I I \int_S \hat{n}_s ds' \quad \hat{n}_s = \hat{n}_s \Rightarrow \vec{S} = \hat{n}_s S$$

TRAŽNI MAGNETI:

atom ~ tokovne zanke



$$\sum_{i=1}^n \vec{p}_{mi} \neq \vec{0}$$

SNOV V ZUNANJEM MAGNETNEM POLJU

Primer: tuljava: $\vec{B} = \frac{\mu_0 N \cdot II}{l} \hat{e}_B$

snov (jedro): magnetizacija
 \Rightarrow dodaten pospešek k \vec{B}

$$\vec{B} \rightarrow \vec{B}' = \mu \vec{B}$$

PERMEABILNOST SNOVI

$$\mu \gg 1 (\sim 3000)$$

FEROMAGNETNE SNOVI

$$\vec{B} = \frac{\mu \cdot \mu_0 N II}{l} \hat{e}_B$$

INDUKTIVNOST (TULJAVE)

IDEJA: $I \rightarrow \vec{B} \rightarrow \Phi_B$ (premikajočise naboji ustvarjajo \vec{B})
 $\Phi_B \propto I$

$$\Phi_B = \pm L I$$

INDUKTIVNOST

Primer: (idealna) tuljava:

$$(a) \vec{B} = \frac{\mu \mu_0 N}{l} II \hat{e}_z (\hat{e}_j \cdot \hat{e}_z)$$

$$(b) I = \int \vec{j}_e \cdot \vec{S}_z = \int \vec{j}_e \cdot \hat{e}_j \cdot \hat{n}_z \cdot S_z = \int \underbrace{\vec{j}_e \cdot \hat{e}_j}_{II} \cdot \hat{e}_j \cdot \hat{n}_z = II (\hat{e}_j \cdot \hat{n}_z)_{\pm 1}$$

$$(\hat{e}_j \cdot \hat{n}_z) I = II (\hat{e}_j \cdot \hat{n}_z) (\hat{e}_j \cdot \hat{n}_z) \Rightarrow II = I (\hat{e}_j \cdot \hat{n}_z)$$

$$\Rightarrow (a) \text{ in } (b): \vec{B} = \frac{\mu \mu_0 N I}{l} \hat{e}_z (\hat{e}_j \cdot \hat{n}_z) (\hat{e}_j \cdot \hat{e}_z)$$

$$(c) \Phi_B = N \vec{B} \cdot \vec{S}_1 = N \frac{\mu \mu_0 N S_1 I}{l} (\hat{e}_j \cdot \hat{n}_z) (\hat{e}_j \cdot \hat{e}_z) (\hat{e}_z \cdot \hat{n}_1)$$

$$L = \frac{\mu \mu_0 N^2 S_1}{l}$$

INDUKTIVNOST (IDEALNE) TULJAVE

$$\left[\frac{Vs m^2}{A m m} = H \right]$$

Henry

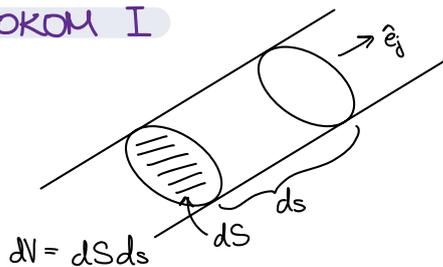
$$\Phi_B = L I (\hat{e}_j \cdot \hat{n}_z) (\hat{e}_j \cdot \hat{e}_z) (\hat{e}_z \cdot \hat{n}_1)$$

MAGNETNA SILA NA VODNIKE S TOKOM I

$$\vec{B}, q, \vec{v} \quad \vec{F}_m = q \vec{v} \times \vec{B}$$

$$d^3q = \rho dV; \quad \rho = nq_1$$

$$d^3F = d^3q \vec{v} \times \vec{B} = \rho \vec{v} \times \vec{B} dV = \int \vec{j}_e \times \vec{B} dV$$



$$dV = dS ds$$

tanka žica:

$\vec{B} \approx \text{konst.}$ na celotnem S

$$\Rightarrow \vec{F} = \int \vec{j}_e \times \vec{B} dV = \int_C \left[\int_S (\vec{j}_e \cdot \hat{e}_j \times \vec{B}) dS \right] ds = \int_C \left[\int_S j dS \right] (\hat{e}_j \times \vec{B}) ds =$$

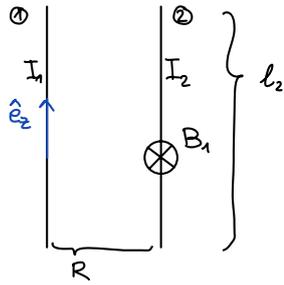
$$= II \int_C \hat{e}_j \times \vec{B} ds = II \int_C d\vec{s} \times \vec{B}; \quad d\vec{s} = \hat{e}_j ds$$

Primer: $\vec{B} = \text{konst.}$, $C = \text{ravna črta}$

$$\rightarrow \vec{F} = I \int_C d\vec{s} \times \vec{B} = I \left[\int_C d\vec{s} \right] \times \vec{B} = I l \vec{l} \times \vec{B}; \quad |\vec{l}| = l \dots \text{dolžina vodnika v } \vec{B}$$

$$\Rightarrow \vec{F} = I l \vec{l} \times \vec{B}$$

Primer:



$$R = 1 \text{ m}$$

$$\hat{e}_{y1} = \hat{e}_{y2} = \hat{e}_z$$

$$|I_1| = |I_2| = I$$

$$l_2 = 1 \text{ m}$$

(a) \vec{B}_1 na mestu 2. vodnika

$$\vec{B}_1 = \frac{\mu_0 I}{2\pi R} \hat{e}_z (\hat{e}_y \cdot \hat{e}_z) =$$

$$= \frac{\mu_0 I}{2\pi R} \hat{e}_z$$

(b) $\vec{l}_2 = l_2 \hat{e}_{y2} = l_2 \hat{e}_z$

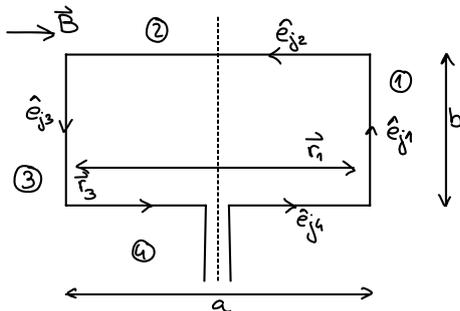
$$\rightarrow \vec{F} = |I_2| \vec{l}_2 \times \vec{B}_1 = I l_2 \hat{e}_z \times \frac{\mu_0 I}{2\pi R} \hat{e}_z = \frac{\mu_0 I^2}{2\pi R} l_2 \underbrace{\hat{e}_z \times \hat{e}_z}_{-\hat{e}_n} = \frac{\mu_0 I^2}{2\pi} \frac{l}{R} (-\hat{e}_n)$$

↑ sila privlačna

• $I = 1 \text{ A} \Rightarrow F = \frac{\mu_0 I^2}{2\pi} = \frac{4\pi \cdot 10^{-7} \text{ Vs A}^2}{2\pi \text{ Am}} = 2 \cdot 10^{-7} \frac{\text{VA s}}{\text{m}}$

NAVOR NA \vec{p}_m (magnetni dipol)

zanika s tokom v homogenem magnetnem polju:



$$\vec{B} = B \hat{e}_x$$

$$\vec{l}_1 = b \hat{e}_y$$

$$\vec{l}_2 = a (-\hat{e}_x)$$

$$\vec{l}_3 = b (-\hat{e}_y)$$

$$\vec{l}_4 = a \hat{e}_x$$

$$\left. \begin{aligned} \vec{F}_1 &= I \vec{l}_1 \times \vec{B} = I l_1 b B \hat{e}_y \times \hat{e}_x = I l_1 b B (-\hat{e}_z) \\ \vec{F}_2 &= 0 \\ \vec{F}_3 &= -\vec{F}_1 = I l_1 b B \hat{e}_z \\ \vec{F}_4 &= 0 \end{aligned} \right\} \Rightarrow \sum \vec{F}_i = 0 \quad \vec{F}_1 = -\vec{F}_3 \dots \text{dvojica sil}$$

$$\vec{r}_1 = \frac{a}{2} \hat{e}_x \quad \text{in} \quad \vec{r}_2 = \frac{a}{2} (-\hat{e}_x)$$

$$\left. \begin{aligned} \vec{M}_1 &= \vec{r}_1 \times \vec{F}_1 = \left(-\frac{a}{2}\right) I l_1 b B \hat{e}_x \times \hat{e}_z = \frac{1}{2} a b I l_1 B \cdot \hat{e}_y \\ \vec{M}_3 &= \vec{r}_3 \times \vec{F}_3 = \frac{1}{2} a b I l_3 B \cdot \hat{e}_y \end{aligned} \right\} \Rightarrow \sum \vec{M}_i = \vec{M}_1 + \vec{M}_3 = a b I l_1 B \hat{e}_y \neq 0$$

$$a b = S \Rightarrow \vec{M} = S I l_1 B \hat{e}_y$$

Spomnimo se: $\vec{p}_m = S I l_1 \hat{n}_s$; $\hat{n}_s \perp \text{ravnina zanike} \Rightarrow \hat{n}_s = \hat{e}_z$

$$\vec{p}_m \times \vec{B} = S I l_1 \hat{e}_z \times B \hat{e}_x = S I l_1 B \hat{e}_z \times \hat{e}_x = S I l_1 B \hat{e}_y = \vec{M}$$

ENERGIJA \vec{p}_m v \vec{B}

2 2 2

MAGNETNA NAPETOST

Elektrostatika: $\vec{\nabla} \cdot \vec{E} = \frac{\rho_e}{\epsilon_0} \oint_{\partial V} \vec{E} d\vec{s}$

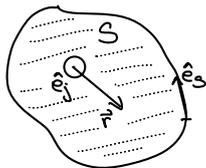
$$\vec{\nabla} \times \vec{E} = 0 \quad \left(\oint_{\partial S} \vec{E} d\vec{s} = 0 \right)$$

Magnetostatika: $\vec{\nabla} \cdot \vec{B} = 0 \quad \left(\oint_{\partial V} \vec{B} d\vec{s} = 0 \right)$

$$\vec{\nabla} \times \vec{B} = ? \quad \left(\oint_{\partial S} \vec{B} d\vec{s} = ? \right)$$

DEFINICIJA: $\oint_C \vec{B} d\vec{s} \equiv \text{MAGNETNA NAPETOST PO } C$

Primer:



$$\oint_{\partial S} \vec{B} d\vec{s} = \int_{t_1}^{t_2} \vec{B} \dot{r} dt$$

Cilindrični koordinatni sistem: $z=0 \Rightarrow \vec{r} = r\hat{e}_n \Rightarrow \dot{\vec{r}} = \dot{r}\hat{e}_n + r\dot{\hat{e}}_n = \dot{r}\hat{e}_n + r\dot{\Phi}\hat{e}_\Phi$

$$\Rightarrow \vec{B} \dot{r} = \frac{\mu_0 I}{2\pi r} \hat{e}_\Phi (r\hat{e}_n + r\dot{\Phi}\hat{e}_\Phi) = \frac{\mu_0 I}{2\pi} \dot{\Phi} \hat{e}_\Phi$$

$$\Rightarrow \oint_{\partial S} \vec{B} d\vec{s} = \frac{\mu_0 I}{2\pi} \int_{t_1}^{t_2} \dot{\Phi} dt = \frac{\mu_0 I}{2\pi} (\Phi(t_2) - \Phi(t_1)) = \mu_0 I$$

↙ če zanka objame vodnik, sicer 0
(n-krat okoli $\Rightarrow \times n$)

$$\oint_{\partial S} \vec{B} d\vec{s} = \mu_0 I$$

↖ zaobjeti tok $\rightarrow I = \int_S \vec{j}_e d\vec{s}$

$$\Rightarrow \oint_{\partial S} \vec{B} d\vec{s} = \mu_0 \int_S \vec{j}_e d\vec{s}$$

$$\oint_{\partial S} \vec{B} d\vec{s} = \int_S (\vec{\nabla} \times \vec{B}) d\vec{s} = \mu_0 \int_S \vec{j}_e d\vec{s}; \forall S \Rightarrow \boxed{\vec{\nabla} \times \vec{B} = \mu_0 \vec{j}_e} \leftarrow \text{IZREK O MAGNETNI NAPETOSTI V DIFERENCIALNI OBLIKI}$$

Predpostavke: 1) $\frac{\partial \rho_e}{\partial t} = 0 \Rightarrow \frac{\partial \rho_e}{\partial t} = -\vec{\nabla} \cdot \vec{j}_e = 0$

2) $\frac{\vec{j}(\vec{r})}{|\vec{r}-\vec{r}'|} \xrightarrow{\vec{r} \rightarrow \infty} 0$

3) $\nabla \int \dots = \int \nabla \dots$

INVARIANCA \vec{p}_m in GALILEJEVE TRANSFORMACIJE

(a) $\vec{F} = m\vec{a}$; v vseh inercialnih opazovalnih sistemih

(b) Galilejeve transformacije: $S, S', \vec{v}_0, \vec{\beta}_0 = \frac{\vec{v}_0}{c}; c_0 = \frac{1}{\sqrt{\mu_0 \epsilon_0}}$
 $t=0: S=S', t=t' \quad (c_0 t = c_0 t')$
 $\vec{r}' = \vec{r} - \vec{v}_0 t = \vec{r} - \vec{\beta}_0 c_0 t$

(c) Galilejeve transformacije: \vec{v} in \vec{a} : $\vec{v} = \frac{d\vec{r}}{dt} \Rightarrow \vec{v}' = \frac{d\vec{r}'}{dt'} = \frac{d\vec{r}}{dt} = \frac{d\vec{r}}{dt} - \frac{d}{dt}(\vec{v}_0 t) = \vec{v} - \vec{v}_0$

$$\vec{a} = \frac{d\vec{v}}{dt} \Rightarrow \vec{a}' = \frac{d\vec{v}'}{dt'} = \frac{d\vec{v}}{dt} = \frac{d\vec{v}}{dt} - \frac{d\vec{v}_0}{dt} = \vec{a} \leftarrow \text{Galilejeva invarianca}$$

(d) Galilejeve transformacije: m in g : $\underline{m}' = m$ in $\underline{g}' = g$ (eksperimentalno dejstvo)

$$\Rightarrow \vec{F} = m\vec{a} = m'\vec{a}' = \vec{F}' \leftarrow \text{Galilejeva invarianca}$$

(e) magnetna sila:

$$\begin{aligned} \text{primer: } S: q, \vec{v}_q, \vec{B} &\rightarrow \vec{F}_m = q\vec{v}_q \times \vec{B} = qc_0 \frac{\vec{v}_q}{c_0} \times \vec{B} = qc_0 \vec{\beta}_q \times \vec{B} \\ S': \vec{v}_0 = \vec{v}_q &\Rightarrow \vec{v}_q' = \vec{v}_q - \vec{v}_0 = 0 \rightarrow \vec{F}_m' = q\vec{v}_q' \times \vec{B}' = 0 \end{aligned} \quad \left. \vphantom{\begin{aligned} \text{primer: } S: q, \vec{v}_q, \vec{B} \\ S': \vec{v}_0 = \vec{v}_q \end{aligned}} \right\} \Rightarrow \vec{F}_m' \neq \vec{F}_m \quad \times$$

Rešitev:

$$(a) \vec{F}_L = \vec{F}_m + \vec{F}_e = q\vec{E} + q\vec{v}_q \times \vec{B} = qc_0 \left(\frac{\vec{E}}{c_0} + \vec{\beta}_q \times \vec{B} \right)$$

$$(b) S: \vec{E} = 0 \Rightarrow \vec{F}_L = qc_0 \vec{\beta}_q \times \vec{B} \quad \vec{v}_q = 0 \quad \vec{\beta}_q = \frac{\vec{v}_q}{c_0} = \frac{\vec{v}_0}{c_0} = \vec{\beta}_0$$

$$S': \vec{E}', \vec{B}' \rightarrow \vec{F}_L' = qc_0 \left(\frac{\vec{E}'}{c_0} + \vec{\beta}_q' \times \vec{B}' \right) = qc_0 \left(\frac{\vec{E}'}{c_0} \right) \quad \vec{\beta}_q' = \frac{\vec{v}_q'}{c_0} = 0$$

$$\rightarrow \vec{F}_L = \vec{F}_L' \Rightarrow \frac{\vec{E}}{c_0} = \vec{\beta}_q \times \vec{B} = \frac{\vec{E}}{c_0} + \vec{\beta}_0 \times \vec{B}$$

BIOT-SAVARTOV ZAKON ZA TOČKASTE NABOJE: q izvor polja (ne testni naboj); \vec{r}_a

$$S: \vec{v}_q = 0, \vec{E}(\vec{r}) = \frac{q}{4\pi\epsilon_0} \frac{\vec{r} - \vec{r}_a}{|\vec{r} - \vec{r}_a|^3}, \vec{B}(\vec{r}) = 0$$

$$S': \vec{v}_0, \vec{v}_q' = \vec{v}_q - \vec{v}_0 = -\vec{v}_0 \quad (\vec{\beta}_q = -\vec{\beta}_0); \vec{B}(\vec{r}) = \vec{v}_q' \times \frac{\mu_0}{4\pi} \frac{\vec{r} - \vec{r}_a}{|\vec{r} - \vec{r}_a|^3} = \frac{\vec{v}_0}{c_0} \times \frac{1}{c_0} \frac{q}{4\pi\epsilon_0} \frac{\vec{r} - \vec{r}_a}{|\vec{r} - \vec{r}_a|^3} = -\vec{\beta}_0 \times \frac{1}{c_0} \vec{E}(\vec{r})$$

$$\rightarrow \vec{B}' = -\vec{\beta}_0 \times \frac{\vec{E}(\vec{r})}{c_0} = \vec{B} - \vec{\beta}_0 \times \frac{\vec{E}}{c_0}$$

Splošno:

$$\vec{F}_L = qc_0 \left(\frac{\vec{E}}{c_0} + \vec{\beta}_q \times \vec{B} \right); \vec{\beta}_q = \frac{\vec{v}_q}{c_0}$$

$$\vec{F}_L' = qc_0 \left(\frac{\vec{E}'}{c_0} + \vec{\beta}_q' \times \vec{B}' \right) =$$

$$= qc_0 \left[\frac{\vec{E}}{c_0} + \vec{\beta}_0 \times \vec{B} + (\vec{\beta}_q - \vec{\beta}_0) \times (\vec{B} - \vec{\beta}_0 \times \frac{\vec{E}}{c_0}) \right] =$$

$$= qc_0 \left[\frac{\vec{E}}{c_0} + \vec{\beta}_0 \times \vec{B} + \vec{\beta}_q \times \vec{B} - \vec{\beta}_0 \times \vec{B} + (\vec{\beta}_q - \vec{\beta}_0) \times (\vec{\beta}_0 \times \frac{\vec{E}}{c_0}) \right] =$$

$$= qc_0 \left[\frac{\vec{E}}{c_0} + \vec{\beta}_q \times \vec{B} + (\vec{\beta}_q - \vec{\beta}_0) \times (\vec{\beta}_0 \times \frac{\vec{E}}{c_0}) \right] =$$

$$= \vec{F}_L + \Delta\vec{F}_L$$

$$\Delta\vec{F}_L = qc_0 (\vec{\beta}_q - \vec{\beta}_0) \times (\vec{\beta}_0 \times \frac{\vec{E}}{c_0}) \neq 0 \quad \uparrow \text{splošnem}$$

$$\text{Velja: } \Delta\vec{F}_L = (\vec{\beta}_q - \vec{\beta}_0) \times (\vec{\beta}_0 \times \vec{F}_L)$$

$$\Rightarrow \vec{F}_L' \neq \vec{F}_L$$

Imamo $f(x, y)$ in $f(x_0, y_0)$. $\Rightarrow f(x, y) = f(x_0, y_0) + \frac{\partial f}{\partial x}(x_0, y_0)(x - x_0) + \frac{\partial f}{\partial y}(x_0, y_0)(y - y_0) + R_2$

$$\Rightarrow f(x, y) \approx f(x_0, y_0) + \frac{\partial f}{\partial x}(x_0, y_0)(x - x_0) + \frac{\partial f}{\partial y}(x_0, y_0)(y - y_0)$$

$$\vec{F}_L' = \vec{F}_L'(\vec{\beta}_q, \vec{\beta}_0) = \begin{bmatrix} F_{L,x}'(\vec{\beta}_q, \vec{\beta}_0) \\ F_{L,y}'(\vec{\beta}_q, \vec{\beta}_0) \\ F_{L,z}'(\vec{\beta}_q, \vec{\beta}_0) \end{bmatrix}$$

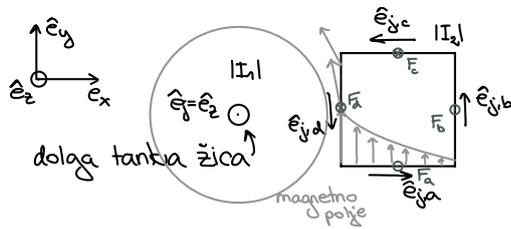
$$F_{L,x}'(\vec{\beta}_q, \vec{\beta}_0) \approx F_{L,x}'(0,0) + \frac{\partial F_{L,x}'}{\partial \beta_{q,x}}(0,0)\beta_{q,x} + \frac{\partial F_{L,x}'}{\partial \beta_{q,y}}(0,0)\beta_{q,y} + \frac{\partial F_{L,x}'}{\partial \beta_{q,z}}(0,0)\beta_{q,z} +$$

$$+ \frac{\partial F_{L,x}'}{\partial \beta_{0,x}}(0,0)\beta_{0,x} + \frac{\partial F_{L,x}'}{\partial \beta_{0,y}}(0,0)\beta_{0,y} + \frac{\partial F_{L,x}'}{\partial \beta_{0,z}}(0,0)\beta_{0,z} = F_{L,x}'(\vec{\beta}_q, \vec{\beta}_0)$$

Podobno: $F'_{1y}(\vec{\beta}_q, \vec{\beta}_o) \approx F_{1y}(\vec{\beta}_q, \vec{\beta}_o)$ in $F'_{1z}(\vec{\beta}_q, \vec{\beta}_o) \approx F_{1z}(\vec{\beta}_q, \vec{\beta}_o)$

F_L : invariančna na Galilejevo transformacijo v linearnem približku; $\beta_q, \beta_o \ll 1$

MAGNETNA SILA in 3. NEWTONOV ZAKON



$\vec{F}_{12} \propto \hat{e}_z$
 $\vec{F}_{21} \perp \hat{e}_z$ } različne smeri
 \Rightarrow ne velja 3. Newtonov zakon

REORGANIZACIJA POGAVAJA

Biot-Savartov zakon: $\vec{B}(\vec{r}) = \int_{\mathbb{R}^3} \frac{\mu_0}{4\pi} \vec{j}(\vec{r}') \times \frac{(\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3} dV'$

\Rightarrow izrek: $\vec{\nabla} \cdot \vec{B} = 0$

\Rightarrow izrek: $\vec{\nabla} \times \vec{B} = \mu_0 \vec{j}$ ($\vec{\nabla} \cdot \vec{j} = 0$, $\frac{\partial \rho}{\partial t} = 0$)

Obrnemo sklepanje:

a) zakon (o magnetnem pretoku): $\vec{\nabla} \cdot \vec{B} = 0$

b) zakon: $\vec{\nabla} \times \vec{B} = \mu_0 \vec{j}$

\Rightarrow Biot-Savartov izrek: $\vec{B}(\vec{r}) = \int_{\mathbb{R}^3} \frac{\mu_0}{4\pi} \vec{j}(\vec{r}') \times \frac{(\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3} dV'$

Dokaz:

Helmholtzov izrek: $\vec{B}(\vec{r}) = -\vec{\nabla} \left[\frac{1}{4\pi} \int_{\mathbb{R}^3} \frac{\vec{\nabla}' \cdot \vec{B}(\vec{r}')}{|\vec{r} - \vec{r}'|} dV' \right] + \vec{\nabla} \times \left[\frac{1}{4\pi} \int_{\mathbb{R}^3} \frac{\vec{\nabla}' \times \vec{B}(\vec{r}')}{|\vec{r} - \vec{r}'|} dV' \right] =$
 $= \vec{\nabla} \times \left[\frac{\mu_0}{4\pi} \int_{\mathbb{R}^3} \frac{\vec{j}(\vec{r}')}{|\vec{r} - \vec{r}'|} dV' \right] = \frac{\mu_0}{4\pi} \int_{\mathbb{R}^3} \vec{\nabla} \times \frac{\vec{j}(\vec{r}')}{|\vec{r} - \vec{r}'|} dV' =$
 $= \frac{\mu_0}{4\pi} \int_{\mathbb{R}^3} \frac{\vec{\nabla} \times \vec{j}(\vec{r}')}{|\vec{r} - \vec{r}'|} - \vec{j}(\vec{r}') \times \nabla \frac{1}{|\vec{r} - \vec{r}'|} dV' =$
 $= \frac{\mu_0}{4\pi} \int_{\mathbb{R}^3} \vec{j}(\vec{r}') \times \frac{(\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3} dV' \quad \square$

POVZETEK II. - IV.

II: $\vec{\nabla} \times \vec{E} = 0$
 $\vec{\nabla} \cdot \vec{E} = \frac{\rho_e}{\epsilon_0}$
 $\vec{E} = q\vec{E}$

III: $\vec{E} = \xi \vec{j}$
 $\frac{\partial \rho}{\partial t} = -\vec{\nabla} \cdot \vec{j}$

IV: $\vec{\nabla} \cdot \vec{B} = 0$
 $\vec{\nabla} \times \vec{B} = \mu_0 \vec{j}$
 $\vec{E} = q \left(\vec{E} + \vec{v}_q \times \vec{B} \right) = qc_0 \left(\frac{\vec{E}}{c_0} + \vec{\beta}_q \times \vec{B} \right)$
 $\vec{E} \approx \frac{c_0}{c} \vec{E} + \vec{\beta}_q \times \vec{B}$
 $\vec{B} \approx \vec{B} - \vec{\beta}_o \times \frac{\vec{E}}{c_0}$

5. ELEKTRODINAMIKA

- (1) $\vec{\nabla} \cdot \vec{E} = \frac{\rho}{\epsilon_0}$... zakon o električnem pretoku ← 1. MAXWELLOVA ENAČBA
- (2) $\vec{\nabla} \times \vec{E} = 0$... zakon o električni napetosti
- (3) $\vec{\nabla} \cdot \vec{B} = 0$... zakon o magnetnem pretoku ← 2. MAXWELLOVA ENAČBA
- (4) $\vec{\nabla} \times \vec{B} = \mu_0 \vec{j}$... zakon o magnetni napetosti

ZAKON O MAGNETNI NAPETOSTI

$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{j} \quad / \vec{\nabla}$$

$$\rightarrow \vec{\nabla}(\vec{\nabla} \times \vec{B}) = \mu_0 \vec{\nabla} \vec{j} \Rightarrow \vec{\nabla} \vec{j} = 0$$

Po drugi strani: $\vec{\nabla} \vec{j} = -\frac{\partial \rho}{\partial t} \neq 0$

$$\Rightarrow \vec{\nabla} \times \vec{B} = \mu_0 \vec{j} \text{ ne velja v splošnem}$$

$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{j} + \vec{G} \quad / \vec{\nabla}$$

$$\rightarrow 0 = \mu_0 \vec{\nabla} \vec{j} + \vec{\nabla} \vec{G} \Rightarrow \vec{\nabla} \vec{G} = -\mu_0 \vec{\nabla} \vec{j} = \mu_0 \frac{\partial \rho}{\partial t}$$

$$\frac{\partial \rho}{\partial t} = \epsilon_0 \frac{\partial}{\partial t} (\vec{\nabla} \cdot \vec{E}) = \epsilon_0 \vec{\nabla} \left(\frac{\partial \vec{E}}{\partial t} \right) =$$

$$\Rightarrow \mu_0 \frac{\partial \rho}{\partial t} = \mu_0 \epsilon_0 \vec{\nabla} \left(\frac{\partial \vec{E}}{\partial t} \right) = \frac{1}{c^2} \vec{\nabla} \left(\frac{\partial \vec{E}}{\partial t} \right)$$

$$\Rightarrow \vec{\nabla} \vec{G} = \frac{1}{c^2} \vec{\nabla} \left(\frac{\partial \vec{E}}{\partial t} \right)$$

$$\Rightarrow \vec{G} = \frac{1}{c^2} \frac{\partial \vec{E}}{\partial t}$$

$$\Rightarrow \vec{\nabla} \times \vec{B} = \mu_0 \vec{j} + \frac{1}{c^2} \frac{\partial \vec{E}}{\partial t} \quad \leftarrow 3. MAXWELLOVA ENAČBA$$

V integralni obliki: $\oint_{\partial S} \vec{B} \cdot d\vec{s} = \int_S (\vec{\nabla} \times \vec{B}) \cdot d\vec{S} = \mu_0 \int_S \vec{j} \cdot d\vec{S} + \frac{1}{c^2} \int_S \frac{\partial \vec{E}}{\partial t} \cdot d\vec{S}$

V primeru, da $S \neq S(t)$: $\int \frac{\partial \vec{E}}{\partial t} \cdot d\vec{S} = \frac{d}{dt} \int \vec{E} \cdot d\vec{S} = \frac{1}{\epsilon_0} \frac{d}{dt} \Phi_E$

$$\vec{\nabla}(\vec{\nabla} \times \vec{B}) = 0 = \mu_0 \vec{\nabla} \vec{j} + \frac{1}{c^2} \vec{\nabla} \left(\frac{\partial \vec{E}}{\partial t} \right) = \mu_0 \vec{\nabla} \vec{j} + \frac{1}{c^2} \frac{\partial}{\partial t} (\vec{\nabla} \cdot \vec{E}) = \mu_0 \vec{\nabla} \vec{j} + \frac{1}{c^2} \frac{1}{\epsilon_0} \frac{\partial}{\partial t} (\rho) = \mu_0 \left(\vec{\nabla} \vec{j} + \frac{\partial \rho}{\partial t} \right) = 0$$

$$\Rightarrow \vec{\nabla} \vec{j} + \frac{\partial \rho}{\partial t} = 0$$

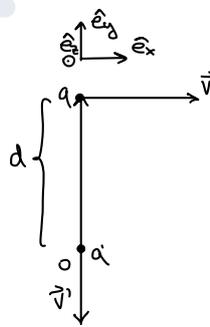
$$\Rightarrow \frac{\partial \rho}{\partial t} = -\vec{\nabla} \vec{j}$$

(III/12) F_L in 3. NEWTONOV ZAKON

(nekaj od prej /dodatek/)

Primer: $q': \vec{r}' = 0$
 $\vec{v}' = v'(-\hat{e}_y)$

$q: \vec{r} = d\hat{e}_y$
 $\vec{v} = v\hat{e}_x$



$\vec{r} - \vec{r}' = d\hat{e}_y$
 $\vec{r}' - \vec{r} = d(-\hat{e}_y)$
 $|\vec{r} - \vec{r}'| = d$

$\vec{E}_q(\vec{r}') = \frac{q}{4\pi\epsilon_0 d^2} \hat{e}_y$
 $\vec{E}_q(\vec{r}) = \frac{q}{4\pi\epsilon_0 d^2} (-\hat{e}_y)$

$\vec{B}_{q'}(\vec{r}') = \frac{1}{c^2} \vec{v}' \times \vec{E}_{q'}(\vec{r}') = \frac{q'v'}{4\pi\epsilon_0 d^2} (-\hat{e}_y) \times \hat{e}_y = 0$
 $\vec{B}_q(\vec{r}') = \frac{1}{c^2} \vec{v} \times \vec{E}_q(\vec{r}') = \frac{qv}{4\pi\epsilon_0 d^2} \hat{e}_x \times (-\hat{e}_y) = \frac{qv}{4\pi\epsilon_0 d^2} (-\hat{e}_z)$

$\vec{F}_e(q' \rightarrow q) = q\vec{E}_{q'} = \frac{qq'}{4\pi\epsilon_0 d^2} \hat{e}_y$
 $\vec{F}_e(q \rightarrow q') = q'\vec{E}_q = \frac{q'q}{4\pi\epsilon_0 d^2} (-\hat{e}_y) = -\vec{F}_e(q' \rightarrow q) \leftarrow$ 3. Newtonov zakon velja

$\vec{F}_m(q' \rightarrow q) = q\vec{v}' \times \vec{B}_{q'} = 0$
 $\vec{F}_m(q \rightarrow q') = q'\vec{v} \times \vec{B}_q = \frac{q'q}{4\pi\epsilon_0 d^2} \frac{v'}{c^2} (-\hat{e}_y) \times (-\hat{e}_z) = \frac{q'q}{4\pi\epsilon_0 d^2} \beta\beta' \hat{e}_x \leftarrow$ 3. Newtonov zakon ne velja

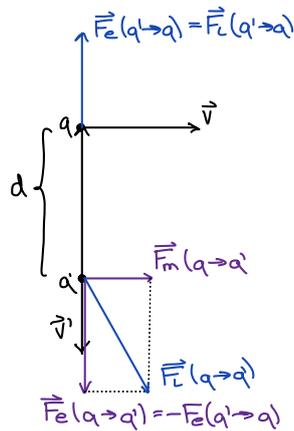
$\vec{F}_L(q' \rightarrow q) \equiv \vec{F}_e(q' \rightarrow q) + \vec{F}_m(q' \rightarrow q)$
 $\vec{F}_L(q \rightarrow q') \equiv \vec{F}_e(q \rightarrow q') + \vec{F}_m(q \rightarrow q')$
 $\Rightarrow \vec{F}_L(q' \rightarrow q) \neq \vec{F}_L(q \rightarrow q')$
 \uparrow 3. Newtonov zakon ne velja.

TEŽAVA: $\int \vec{F}_L(q' \rightarrow q) dt = \Delta \vec{G}_q = \vec{G}_{qk} - \vec{G}_{qz}$

(sredk sil) $\int \vec{F}_L(q \rightarrow q') dt = \Delta \vec{G}_{q'} = \vec{G}_{q'k} - \vec{G}_{q'z} \neq -(\vec{G}_{qk} - \vec{G}_{qz})$

$\vec{G}_{qk} - \vec{G}_{qz} + \vec{G}_{q'k} - \vec{G}_{q'z} = \vec{G}_{qk} + \vec{G}_{q'k} - (\vec{G}_{qz} + \vec{G}_{q'z}) = \vec{G}_k - \vec{G}_z$
 $\neq \vec{G}_{qk} - \vec{G}_{qz} - (\vec{G}_{q'k} - \vec{G}_{q'z}) = 0^* \Rightarrow \boxed{\vec{G}_k \neq \vec{G}_z}$

↑ skupna gibalna količina se ne ohranja

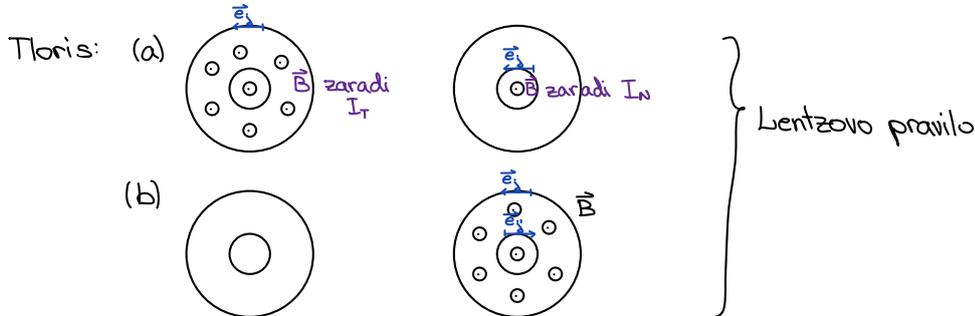


ZAKON O ELEKTRIČNI NAPETOSTI

$$\vec{\nabla} \times \vec{E} = 0$$

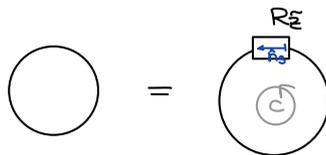
Poskus: Faradaj

Kvalitativno: vključimo/izključimo I
 \Rightarrow spremenijo se \vec{B} ; $\frac{\partial \vec{B}}{\partial t} \neq 0$
 $\Rightarrow \frac{\partial \vec{B}}{\partial t} \neq 0 \rightarrow$ se obda z $\vec{E} \Rightarrow$ požene I_w



Poskus v nasprotju z: $\vec{\nabla} \times \vec{E} = 0$ in $\vec{E} = \epsilon \vec{j}$

o notranja zanka:



$$\Rightarrow U = -I R_E \neq 0$$

$$\vec{\nabla} \times \vec{E} = 0$$

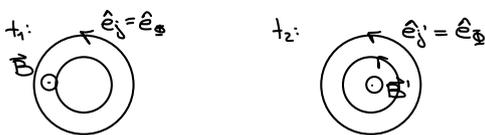
$$\Rightarrow \int (\vec{\nabla} \times \vec{E}) d\vec{S} = 0$$

$$\Rightarrow \oint_{\partial S} \vec{E} d\vec{s} = \int (\vec{\nabla} \times \vec{E}) d\vec{S} = 0 = -U$$

$$\Rightarrow U = 0$$

$$\Rightarrow \vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} \leftarrow 4. \text{ MAXWELLOVA ENAČBA}$$

$$\int_S (\vec{\nabla} \times \vec{E}) d\vec{S} = - \int \frac{\partial \vec{B}}{\partial t} d\vec{S} = \oint_{\partial S} \vec{E} d\vec{s} \leftarrow \text{integralna oblika}$$



a) $\vec{B}(t_1) = B \hat{e}_z$ $B(t_2) = 0$
 $\Rightarrow \Delta \vec{B} = \vec{B}(t_2) - \vec{B}(t_1) = B(-\hat{e}_z)$
 $\Rightarrow \frac{\partial \vec{B}}{\partial t} \propto (-\hat{e}_z) \Rightarrow -\frac{\partial \vec{B}}{\partial t} \propto \hat{e}_z \Rightarrow \vec{E} \propto \hat{e}_\phi$

$$\hat{e}_\phi = \sin \Phi \hat{e}_x + \cos \Phi \hat{e}_y$$

$$\sin \Phi = \frac{y}{r}$$

$$\cos \Phi = \frac{x}{r}$$

$$r = \sqrt{x^2 + y^2}$$

$$\rightarrow \frac{\partial}{\partial x} (\sin \Phi) = \frac{xy}{r^3}$$

$$\frac{\partial}{\partial y} (\sin \Phi) = \frac{1}{r} - \frac{y^2}{r^3}$$

$$\frac{\partial}{\partial z} (\sin \Phi) = 0$$

$$\frac{\partial}{\partial x} (\cos \Phi) = \frac{1}{r} - \frac{x^2}{r^3}$$

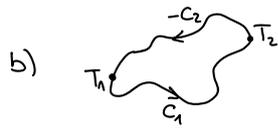
$$\frac{\partial}{\partial y} (\cos \Phi) = \frac{xy}{r^3}$$

$$\frac{\partial}{\partial z} (\cos \Phi) = 0$$

$$\vec{\nabla} \times \vec{E} \propto \vec{\nabla} \times \hat{e}_\phi = \left(\frac{\partial}{\partial y} 0 - \frac{\partial}{\partial z} \sin \Phi \right) \hat{e}_x + \left(-\frac{\partial}{\partial z} (\sin \Phi) - \frac{\partial}{\partial x} 0 \right) \hat{e}_y + \left(\frac{\partial}{\partial x} (\cos \Phi) + \frac{\partial}{\partial y} (\sin \Phi) \right) \hat{e}_z =$$

$$= \left(\frac{1}{r} - \frac{x^2}{r^3} + \frac{1}{r} - \frac{y^2}{r^3} \right) \hat{e}_z = \left(\frac{2}{r} - \frac{x^2 + y^2}{r^3} \right) \hat{e}_z = \left(\frac{2}{r} - \frac{1}{r} \right) \hat{e}_z = \frac{1}{r} \hat{e}_z$$

Komentarji: a) $\vec{\nabla} \times \vec{E} \neq 0 \Rightarrow -\oint_{\partial S} \vec{E} d\vec{s} = \int_S \frac{\partial \vec{B}}{\partial t} d\vec{S} \neq 0$ (V nasprotju z 2. Kirchoffovim izrekom)



$$\partial S = C_1 + (-C_2)$$

$$\oint_{\partial S} \vec{E} d\vec{s} = \int_{C_1} \vec{E} d\vec{s} + \int_{-C_2} \vec{E} d\vec{s} = \int_{C_1} \vec{E} d\vec{s} - \int_{C_2} \vec{E} d\vec{s} \neq 0$$

$$\Rightarrow \int_{C_1} \vec{E} d\vec{s} \neq \int_{C_2} \vec{E} d\vec{s}$$

c) $-U(T_1 \rightarrow T_2; C_1) \neq -U(T_1 \rightarrow T_2; C_2)$

$U(T_1 \rightarrow T_2) = U(C)$ ← funkcija poti

$$\vec{\nabla} \times \vec{E} = 0 \wedge \frac{\partial \vec{B}}{\partial t} = 0$$

d) Potenciali: $\vec{B} = \vec{\nabla} \times \vec{A} \Rightarrow \vec{\nabla} \cdot \vec{B} = 0$

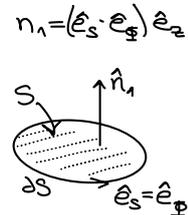
$$\vec{E} = -\vec{\nabla} \Phi \Rightarrow \vec{\nabla} \times \vec{E} = 0 //$$

$$\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} = -\frac{\partial}{\partial t} (\vec{\nabla} \times \vec{A}) = \vec{\nabla} \times \left(-\frac{\partial \vec{A}}{\partial t} \right) //$$

$$\Rightarrow \vec{E} = -\vec{\nabla} \Phi - \frac{\partial \vec{A}}{\partial t}$$

IV/6.:

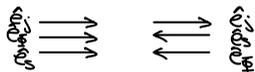
$$\begin{aligned} \text{Za en ovoj: } \underbrace{-\oint_{\partial S} \vec{E} d\vec{s}}_{\text{Stokes}} &= -\int_{S_1} (\vec{\nabla} \times \vec{E}) d\vec{S} \\ &= \int_{S_1} \frac{\partial \vec{B}}{\partial t} d\vec{S} \quad (\text{Maxwell}) \\ &= \frac{\partial}{\partial t} \int_{S_1} \vec{B} d\vec{S} \quad (S_1 \neq S_1(t)) \\ &= \frac{\partial}{\partial t} \Phi_B \end{aligned}$$



Spomnimo se: $\Phi_B = LI(\hat{e}_j \cdot \hat{e}_\phi)(\hat{e}_j \cdot \hat{n}_z)(\hat{e}_z \cdot \hat{n}_1)$; $L = \frac{\mu \mu_0 N^2 S_1}{l}$
 $= LI(\hat{e}_j \hat{e}_\phi)(\hat{e}_j \hat{n}_z)(\hat{e}_z \hat{e}_z)(\hat{e}_s \hat{e}_\phi)$
 $= LI(\hat{e}_j \hat{e}_\phi)(\hat{e}_j \hat{n}_z)(\hat{e}_s \hat{e}_\phi)$

a) $\hat{n}_z = +\hat{e}_s$:
 $(\hat{e}_j \hat{e}_\phi)(\hat{e}_j \hat{e}_s)(\hat{e}_s \hat{e}_\phi) = +1$

b) $\hat{n}_z = -\hat{e}_s$:
 $(\hat{e}_j \hat{e}_\phi)(\hat{e}_j (-\hat{e}_s))(\hat{e}_s \hat{e}_\phi) = -1$



$$\Rightarrow \Phi_B = \begin{cases} LI; & \hat{n}_z = \hat{e}_s \\ -LI; & \hat{n}_z = -\hat{e}_s \end{cases}$$

2. KIRCHHOFFOV IZREK (drugič)

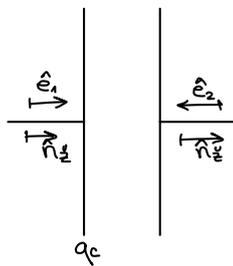
- spremenljiva U in I
- C, L

a) Napetost na L :
 ◦ napetost odvisna od poti: skozi tuljavo
 ◦ žice tuljave: idealno prevodne: $\xi \rightarrow 0 \Rightarrow \vec{E} = \xi \vec{j} \rightarrow \vec{E} \rightarrow 0$

$$\Rightarrow U_L = -\int_C \vec{E} d\vec{s} = 0$$

b) Napetost na kondenzatorju:

- izberemo \hat{n}_z
- $q_c \equiv$ naboj na plošči, proti kateri kaže \hat{n}_z
- III/4: $I = \frac{dq_c}{dt}$
- izberemo smer obhoda



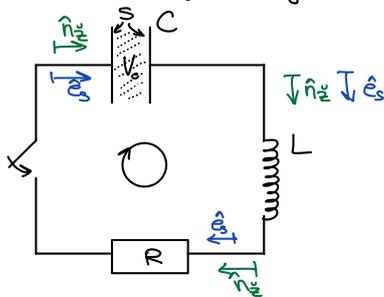
$$U_c = - \int \vec{E} d\vec{s}$$

↖ od ene do druge plošče

- e_1 : $q_c > 0 \Rightarrow \vec{E} > 0$; $\vec{E} \hat{e}_1 > 0$
 $U_c < 0 \Rightarrow U_c = -\frac{q_c}{C}$
- $q_c < 0 \Rightarrow \vec{E} < 0$; $\vec{E} \hat{e}_1 < 0$
 $U_c > 0 \Rightarrow U_c = -\frac{q_c}{C}$
- e_2 : $U_c = \frac{q_c}{C}$

$$\Rightarrow U_c = \begin{cases} -\frac{q_c}{C} & ; e_1 \hat{n}_z = 1 \\ \frac{q_c}{C} & ; e_1 \hat{n}_z = -1 \end{cases}$$

Primer: električni nihajni krog



$$t=0: \begin{aligned} q_c(t=0) &= q_0 \\ I(t=0) &= 0 \end{aligned}$$

$$\oint \vec{E} d\vec{s} = \frac{d}{dt} \Phi_B$$

$$U_c + U_L + U_R = \frac{d}{dt} \Phi_B \quad (\sum U \neq 0)$$

$$U_L = 0; U_c = -\frac{q_c}{C}; U_R = -IR; \frac{d}{dt} \Phi_B = LI$$

$$\Rightarrow -\frac{q_c}{C} - IR = LI; \dot{I} = \ddot{q}_c$$

$$\Rightarrow -\frac{q_c}{C} - \dot{q}_c R = L \ddot{q}_c$$

$$L \neq 0 \Rightarrow \ddot{q}_c + \beta \dot{q}_c + \omega_0^2 q_c = 0; \beta = \frac{R}{L}, \omega_0^2 = \frac{1}{LC}$$

↖ enačba dušenega nihanja

$$\hookrightarrow q_c = A e^{-\beta t} \sin(\omega t + \delta); \omega = \sqrt{\omega_0^2 - \frac{\beta^2}{4}}$$

$$(1) L=0: \ddot{q}_c + \frac{q_c}{C} = 0; \tau = RC [s]$$

$$q_c(t) = q_0 \exp\left\{-\frac{t}{\tau}\right\}$$

$$\Rightarrow I = \dot{q}_c = -\frac{q_0}{\tau} \exp\left\{-\frac{t}{\tau}\right\}$$

$$\text{Spomnimo se: } P_{el} = I_R^2 R = R I_0^2 \exp\left\{-\frac{2t}{\tau}\right\}$$

$$A_{el} = \int_0^\infty P_{el} dt = \dots = \frac{q_0^2}{2C} \Rightarrow \Delta W_h > 0 \Rightarrow \Delta W_R > 0$$

$$\Delta W = 0 \Rightarrow \Delta W_c + \Delta W_R = 0 \Rightarrow \Delta W_c = -\Delta W_R = -\frac{q_0^2}{2C}$$

$$W_c := \frac{q_c^2}{2C} = \frac{1}{2} \frac{(CU_c)^2}{C} = \frac{CU_c^2}{2} = \frac{1}{2} \frac{\epsilon_0 S E^2 l^2}{l} = \frac{1}{2} S l \epsilon_0 E^2 = \frac{1}{2} V \epsilon_0 E^2 \quad (V = V_c \approx V_E)$$

volumen električnega polja

$$= \frac{1}{2} V \epsilon_0 E^2 =: W_E$$

$$W_E = V \frac{1}{2} \epsilon \epsilon_0 E^2$$

(2) $R=0$: $L\ddot{q}_c + \frac{q_c}{C} = 0 \rightarrow \ddot{q}_c + \omega_0^2 q_c = 0$; $\omega_0^2 = \frac{1}{LC}$ [s⁻²]

← ENAČBA NEDUŠENEGA NIHANJA

$$q_c = A \sin(\omega_0 t + \delta)$$

$$I = A \omega_0 \cos(\omega_0 t + \delta)$$

$$\begin{aligned} (1) \quad q_c(t=0) = q_0 &\Rightarrow q_0 = A \sin \delta \\ (2) \quad I(t=0) = 0 &\Rightarrow 0 = A \omega_0 \cos \delta \end{aligned} \Rightarrow \omega_0 \cot \delta = 0 \Rightarrow \delta = \frac{\pi}{2}$$

$$\Rightarrow q_0 = A$$

$$\Rightarrow \begin{cases} q_c = q_0 \cos(\omega_0 t) \\ I = -I_0 \sin(\omega_0 t) \end{cases}; \quad I_0 = q_0 \omega_0$$

$$\begin{aligned} t=0: \quad W_c (= W_E) &= \frac{1}{2} \frac{q_c^2}{C} \\ t = \frac{\pi}{2\omega_0}: \quad W_c (= W_E) &= 0 \end{aligned} \Rightarrow \Delta W_c = -\frac{1}{2} \frac{q_0^2}{C}$$

$$\Delta W = 0$$

$$\Delta W = \Delta W_c + \Delta W_L = 0$$

$$\Rightarrow \Delta W_L = -\Delta W_c = \frac{1}{2} \frac{q_0^2}{C} = \frac{1}{2} \frac{I_0^2}{C \omega_0^2} = \frac{1}{2} \frac{L I_0^2}{C} = \frac{1}{2} L I_0^2$$

$$\Rightarrow W_L = \frac{1}{2} L I_0^2 =$$

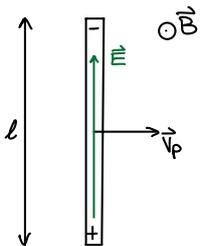
$$B = \frac{\mu_0 \mu N I}{l} \rightarrow I = \frac{B l}{\mu \mu_0 N} \rightarrow W_L = \frac{1}{2} \frac{\mu \mu_0 N^2 S}{l} \frac{l^2 B^2}{(\mu \mu_0)^2 N^2} = \frac{1}{2} S l \frac{B^2}{\mu \mu_0} = \frac{1}{2} V_B \frac{B^2}{\mu \mu_0} = W_B$$

↑
prostorna magnetnega polja

Gostota energij: $W_E = \frac{W_E}{V_E} = \frac{1}{2} \epsilon \epsilon_0 E^2$

$$W_B = \frac{W_B}{V_B} = \frac{1}{2} \frac{B^2}{\mu \mu_0}$$

"INDUKCIJA" (NAVIDEZNA INDUKCIJA) (Laurentsova sila)



$$\vec{B} = B \hat{e}_z; \quad B > 0$$

$$\vec{v}_p = v_p \hat{e}_x; \quad v_p > 0$$

$$e^-: \quad q_1 = -q_0$$

$$\vec{F}_m = q \vec{v} \times \vec{B} = -q_0 v_p \vec{B} \hat{e}_x \times \hat{e}_z = q_0 v_p B \hat{e}_y$$

$$\vec{F}_e = q \vec{E} = -q_0 E \hat{e}_y = q_0 E (-\hat{e}_y)$$

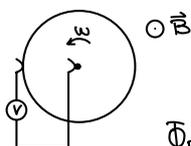
$$\vec{F}_m + \vec{F}_e = 0$$

$$q_0 v_p B \hat{e}_y + q_0 E (-\hat{e}_y) = 0 \rightarrow E = v_p B \rightarrow U = \pm E l = \pm v_p B l$$

$$U = \vec{v}_p \cdot (\vec{B} \times \vec{l}); \quad \vec{l} = l \hat{e}_z$$

$$U = \int \vec{v}_p \cdot (\vec{B} \times d\vec{l})$$

Faradjev disk:

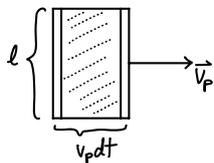


$$\Phi_B \neq \Phi_B(t)$$

$$\Rightarrow \frac{d\Phi_B}{dt} \neq 0$$



$$U = \frac{1}{2} \omega B l^2$$



$$dS = l v_p dt$$

$$d\Phi_B = B dS = v_p B l dt \quad v_p B l = \frac{d\Phi_B}{dt} = U (\neq U_i)$$

$$-\oint_{\partial S} \vec{E} \cdot d\vec{s} = \int_S \frac{\partial \vec{B}}{\partial t} \cdot d\vec{S} \quad U_i = \int \frac{\partial \vec{B}}{\partial t} \cdot d\vec{S} ; S = S(t)$$

$$= \frac{d}{dt} \int \vec{B} \cdot d\vec{S} = \frac{d}{dt} \Phi_B$$

ELEKTROMAGNETNO VALOVANJE

Maxwellove enačbe: $\vec{\nabla} \cdot \vec{B} = 0$ $\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$

$$\vec{\nabla} \cdot \vec{E} = \frac{\rho}{\epsilon_0} \quad \vec{\nabla} \times \vec{B} = \mu_0 \vec{j} + \frac{1}{c^2} \frac{\partial \vec{E}}{\partial t} ; c_0 = \frac{1}{\sqrt{\mu_0 \epsilon_0}} \approx 3 \cdot 10^8 \frac{m}{s}$$

Za prazen prostor: $\rho = 0$ $\vec{j} = 0$

$$\left. \begin{array}{l} \rho = 0 \\ \vec{j} = 0 \end{array} \right\} \Rightarrow \vec{\nabla} \cdot \vec{B} = 0 \quad \vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\vec{\nabla} \cdot \vec{E} = 0 \quad \vec{\nabla} \times \vec{B} = \frac{1}{c^2} \frac{\partial \vec{E}}{\partial t}$$

Matematična resnica: \vec{E} poljubno: $\vec{\nabla} \times (\vec{\nabla} \times \vec{E}) = \vec{\nabla}(\vec{\nabla} \cdot \vec{E}) - \nabla^2 \vec{E}$; $\nabla^2 = (\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2})$

$$\rightarrow \vec{\nabla} \times (\vec{\nabla} \times \vec{E}) = -\vec{\nabla} \times \left(\frac{\partial \vec{B}}{\partial t} \right)$$

$$\underbrace{\vec{\nabla}(\vec{\nabla} \cdot \vec{E}) - \nabla^2 \vec{E}}_0 = -\frac{\partial}{\partial t} (\vec{\nabla} \times \vec{B})$$

$$= -\frac{\partial}{\partial t} \left(\frac{1}{c^2} \frac{\partial \vec{E}}{\partial t} \right) \Rightarrow -\nabla^2 \vec{E} = -\frac{1}{c^2} \frac{\partial^2 \vec{E}}{\partial t^2} \rightarrow \boxed{\nabla^2 \vec{E} = \frac{1}{c^2} \frac{\partial^2 \vec{E}}{\partial t^2}}$$

$$\rightarrow \boxed{\nabla^2 \vec{B} = \frac{1}{c^2} \frac{\partial^2 \vec{B}}{\partial t^2}}$$

Komentarji:

1) elektromagnetno valovanje (potovanje motnje v \vec{E} in \vec{B}) se lahko širi skozi prazen prostor

2) c ... hitrost razširjanja motnje
 $c_0 = \text{konst. (!?)}$

\hookrightarrow ne ujema se z Galilejevimi transformacijami:

$$S: \vec{v} = c_0 \hat{e}_x$$

$$S': \vec{v}_0 = v_0 \hat{e}_x$$

$$GT: \vec{v}' = \vec{v} - \vec{v}_0 = (c_0 - v_0) \hat{e}_x =$$

$$= c_0 (1 - \beta_0) \hat{e}_x ; \beta_0 = \frac{v_0}{c_0} \quad *$$

$\vec{E} \perp \vec{B} \perp \vec{z}$. (EM valovanje: transverzalno)

$$B = \frac{E}{c_0}$$

$$W_E = \frac{1}{2} \epsilon_0 E^2 \quad W_B = \frac{1}{2} \frac{B^2}{\mu_0} = \frac{1}{2} \frac{E^2}{\mu_0 c_0^2} = \frac{\epsilon_0 \mu_0 E^2}{2 \mu_0} = \frac{1}{2} \epsilon_0 E^2 = W_E$$

$$W = W_E + W_B = \epsilon_0 E^2$$

$$\vec{j}_{em} = W \vec{z} = \epsilon_0 E^2 \vec{z} ; \mathcal{P} = \vec{E} \times \frac{\vec{B}}{\mu_0} = \vec{j}$$

\uparrow Poyntingov vektor

6. POSEBNA TEORIJA RELATIVNOSTI

INVENTURA

Maxwellove enačbe:

$$\begin{aligned}\vec{\nabla} \cdot \vec{B} &= 0 \\ \vec{\nabla} \cdot \vec{E} &= \frac{\rho}{\epsilon_0} \\ \vec{\nabla} \times \vec{E} &= -\frac{\partial \vec{B}}{\partial t} \\ \vec{\nabla} \times \vec{B} &= \mu_0 \vec{j} + \frac{1}{c^2} \frac{\partial \vec{E}}{\partial t}\end{aligned}$$

Ohmov zakon: $\vec{E} = \zeta \vec{j}$

Lorentzova sila: $\vec{F}_L = q c_0 \left(\frac{\vec{E}}{c_0} + \vec{\beta}_v \times \vec{B} \right); \quad \vec{\beta}_v = \frac{\vec{v}_v}{c_0}$

Galilejeve transformacije: $S \rightarrow S', \vec{v}_0$

$$\begin{aligned}c_0 t' &= c_0 t \\ \vec{r}' &= \vec{r} - \vec{\beta}_0 c_0 t; \quad \vec{\beta}_0 = \frac{\vec{v}_0}{c_0}\end{aligned}$$

Transformacije \vec{E} in \vec{B} :

$$\begin{aligned}\frac{\vec{E}'}{c_0} &= \frac{\vec{E}}{c_0} + \vec{\beta}_0 \times \vec{B} \\ \vec{B}' &= \vec{B} - \vec{\beta}_0 \times \frac{\vec{E}}{c_0}\end{aligned}$$

TEŽAVE: • $\vec{F}_L' \neq \vec{F}_L$ (težave v linearnem približku glede na $\vec{\beta}_0$ ni)

• EM valovanje: hitrost = $c_0 = \frac{1}{\sqrt{\mu_0 \epsilon_0}} = \text{konst.}$
(v nasprotju z Galilejevimi transformacijami že v linearnem približku)

GALILEJEVE TRANSFORMACIJE (ponovitev)

$S, S'; \vec{v}_0 = \text{konst.}$
↗
nepospešena sistema

$$\left. \begin{aligned}\vec{r}: O \rightarrow T \\ \vec{r}': O' \rightarrow T\end{aligned} \right\} \vec{r}' = \vec{r} - \vec{v}_0 t = \vec{r} - \vec{\beta}_0 c_0 t = \vec{r}' \\ c_0 t' = c_0 t$$

$\vec{v}_0 = v_0 \hat{e}_x$ (gibanje sistema vzdolž x-osi glede na drugega)

$$\begin{aligned}c_0 t' &= c_0 t \\ x' &= x - \beta_0 c_0 t; \quad \beta_0 = \frac{v_0}{c_0} \\ y' &= y \\ z' &= z\end{aligned}$$

4-dimenzionalni vektor prostor-čas: ${}^4X = \begin{bmatrix} c_0 t \\ \vec{r} \end{bmatrix} = \begin{bmatrix} c_0 t \\ x \\ y \\ z \end{bmatrix}; \quad {}^4X' = \begin{bmatrix} c_0 t' \\ \vec{r}' \end{bmatrix} = \begin{bmatrix} c_0 t' \\ x' \\ y' \\ z' \end{bmatrix}$

$$G = \begin{bmatrix} 1 & 0 & 0 & 0 \\ -\beta_0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \quad G^{-1} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ \beta_0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \quad GG^{-1} = G^{-1}G = \mathbb{1}_{4 \times 4}$$

$$\boxed{{}^4X = G^{-1} {}^4X'}$$

GALILEJEVE TRANSFORMACIJE HITROSTI:

$$\vec{v} = \frac{d\vec{r}}{dt} = \begin{bmatrix} v_x \\ v_y \\ v_z \end{bmatrix}; \quad v_x = \frac{dx}{dt}, \quad v_y = \frac{dy}{dt}, \quad v_z = \frac{dz}{dt}$$

$$\Rightarrow v_x' = \frac{dx'}{dt'} = \frac{dx'}{dt} = \frac{d}{dt} (x - \beta_0 c_0 t) = v_x - \beta_0 c_0 = v_x - v_0$$

$$v_y' = \frac{dy'}{dt'} = \frac{dy'}{dt} = v_y \quad v_z' = v_z$$

Primer: $S: \vec{v} = c_0 \hat{e}_x, \boxed{v = c_0 = v_x}$

$S':$ GT: $v_x' = c_0 - v_0$

$v_y' = v_y = 0$

$v_z' = v_z = 0$

$\boxed{v' = v_x' = c_0 - v_0 = c_0(1 - \beta_0)}$

- 2x narobe: • Maxwellove enačbe ✖
• eksperimenti ✖

LORENTZOVE TRANSFORMACIJE

$$\begin{cases} ct' = \gamma_0(ct - \beta_0 x) \\ x' = \gamma_0(x - \beta_0 ct) \\ y' = y \\ z' = z \end{cases} \leftarrow \text{LORENTZOVE TRANSFORMACIJE}$$

$\beta_0 = \frac{v_0}{c_0}$ in $\gamma_0 = \frac{1}{\sqrt{1 - \beta_0^2}}$

KOMENTARJI:

(1) $\beta_0^2 \geq 0 \Rightarrow \gamma_0 \geq 1$

(a) $v_0 \rightarrow c_0 \Rightarrow \beta_0 \rightarrow 1 \Rightarrow \gamma_0 \rightarrow \infty$

(b) $v_0 \ll c_0 \Rightarrow \beta_0^2 \ll 1 \Rightarrow \gamma_0 = \frac{1}{\sqrt{1 - \beta_0^2}} \approx \frac{1}{1 - \frac{1}{2}\beta_0^2} \approx 1 + \frac{1}{2}\beta_0^2 \Rightarrow \gamma_0 - 1 \approx \frac{1}{2}\beta_0^2$

$$\boxed{ct' = \gamma_0(ct - \beta_0 x)} = ct - \beta_0 x + (\gamma_0 - 1)(ct - \beta_0 x)$$

$$\approx ct - \beta_0 x + \frac{1}{2}\beta_0^2(ct - \beta_0 x)$$

$\approx ct - \beta_0 x$

$\rightarrow \boxed{x' \approx x - \beta_0 ct}$

zaradi tega pogosta napaka v linearnem približku

Lorentzove transformacije

(2) $ct = \gamma_0(ct - \beta_0 x) \Rightarrow t' = \gamma_0(t - \frac{\beta_0}{c_0} x) \neq t$

MATRIČNI ZAPIS:

$$\Lambda = \begin{bmatrix} \gamma_0 & -\beta_0 \gamma_0 & 0 & 0 \\ \beta_0 \gamma_0 & \gamma_0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\Lambda^{-1} = \begin{bmatrix} \gamma_0 & \beta_0 \gamma_0 & 0 & 0 \\ \beta_0 \gamma_0 & \gamma_0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$\boxed{{}^4X' = \Lambda {}^4X}$ in $\boxed{{}^4X = \Lambda^{-1} {}^4X'}$

Definicija: 4-dimenzionalni vektor je VEKTOR-ČETVEREC ali ŠTIRIVEKTOR, če se transformira pri prehodu $S \rightarrow S'$ z množenjem z Λ .

$\Lambda \rightarrow \Lambda^{-1} \Leftrightarrow \vec{v}_0 \rightarrow -\vec{v}_0$

$$\begin{cases} ct = \gamma_0(ct' + \beta_0 x') \\ x = \gamma_0(x' + \beta_0 ct') \\ y = y' \\ z = z' \end{cases}$$

LORENTZOVE TRANSFORMACIJE HITROSTI:

$v_x = \frac{dx}{dt} \Rightarrow v_x' = \frac{dx'}{dt'} = \frac{dx'}{dt} \frac{dt}{dt'} = \frac{dx'}{dt} / \frac{dt}{dt'}$

$\frac{dx'}{dt} = \frac{\partial x'}{\partial t} + \frac{\partial x'}{\partial x} \frac{dx}{dt} = \frac{\partial x'}{\partial t} + v_x \frac{\partial x'}{\partial x}$

$x' = \gamma_0(x - \beta_0 ct) \Rightarrow \frac{\partial x'}{\partial t} = -\gamma_0 \beta_0 c_0 = -\gamma_0 v_0; \frac{\partial x'}{\partial x} = \gamma_0$

$\Rightarrow \gamma_0(v_x - v_0) = \frac{dx'}{dt}$

$\Rightarrow v_x' = \frac{v_x - v_0}{1 - \frac{v_x v_0}{c_0^2}}$

$\frac{dt'}{dt} = \frac{\partial t'}{\partial t} + \frac{\partial t'}{\partial x} \frac{dx}{dt} = \frac{\partial t'}{\partial t} + v_x \frac{\partial t'}{\partial x}$

$t' = \gamma_0(t - \frac{\beta_0}{c_0} x) \Rightarrow \frac{\partial t'}{\partial t} = \gamma_0; \frac{\partial t'}{\partial x} = -\frac{\gamma_0 \beta_0}{c_0}$

$\Rightarrow \frac{dt'}{dt} = \gamma_0(1 - \frac{v_x v_0}{c_0^2})$

$$v_y' = \frac{dy'}{dt'} = \frac{dy'}{dt} \frac{dt}{dt'} = \frac{dy'}{dt} / \frac{dt}{dt'} = \frac{dy'}{dt} / \frac{dt'}{dt} = \frac{1}{\gamma} \frac{v_y}{(1 - \frac{v_x v_0}{c^2})}$$

$$v_z' = \frac{1}{\gamma} \frac{v_z}{(1 - \frac{v_x v_0}{c^2})}$$

$$v^2 = v_x^2 + v_y^2 + v_z^2$$

$$\begin{aligned} v'^2 = v_x'^2 + v_y'^2 + v_z'^2 &= \left[(v_x - v_0)^2 + \frac{v_y^2 + v_z^2}{\gamma^2} \right] / \left(1 - \frac{v_x v_0}{c^2} \right)^2 = \left[v_x^2 + v_0^2 - 2v_x v_0 + (1 - \beta_0^2)(v_y^2 + v_z^2) \right] / \left(1 - \frac{v_x v_0}{c^2} \right)^2 = \\ &= \left[v_x^2 + v_y^2 + v_z^2 - \beta_0^2(v_y^2 + v_z^2) + v_0^2 - 2v_x v_0 \right] / \left(1 - \frac{v_x v_0}{c^2} \right)^2 = \\ &= \left[v^2 - \beta_0^2 v_x^2 + \beta_0^2 v_x^2 - \beta_0^2(v_y^2 + v_z^2) + v_0^2 - 2v_x v_0 \right] / \left(1 - \frac{v_x v_0}{c^2} \right)^2 = \\ &= \left[v^2(1 - \beta_0^2) + v_x^2 \beta_0^2 - 2v_x v_0 + v_0^2 \right] / \left(1 - \frac{v_x v_0}{c^2} \right)^2 = \\ \beta^2 = \frac{v'^2}{c^2} &\rightarrow = c^2 \left[\beta^2(1 - \beta_0^2) + \frac{v_x^2 v_0^2}{c^4} - \frac{2v_x v_0}{c^2} + \frac{v_0^2}{c^2} \right] / \left(1 - \frac{v_x v_0}{c^2} \right)^2 = \\ &= c^2 \left[\beta^2(1 - \beta_0^2) + \frac{v_x^2 v_0^2}{c^4} - \frac{2v_x v_0}{c^2} + 1 - 1 + \beta_0^2 \right] / \left(1 - \frac{v_x v_0}{c^2} \right)^2 = \\ &= c^2 \left[\beta^2(1 - \beta_0^2) + \left(1 - \frac{v_x v_0}{c^2} \right)^2 - (1 - \beta_0^2) \right] / \left(1 - \frac{v_x v_0}{c^2} \right)^2 = \\ &= c^2 \left[(1 - \beta_0^2)(\beta^2 - 1) + \left(1 - \frac{v_x v_0}{c^2} \right)^2 \right] / \left(1 - \frac{v_x v_0}{c^2} \right)^2 = \\ &= c^2 \left[1 - \frac{(1 - \beta_0^2)(1 - \beta^2)}{\left(1 - \frac{v_x v_0}{c^2} \right)^2} \right] \end{aligned}$$

Primer: S: $v = c_0$; $v' = ?$
 $\Rightarrow \beta^2 = \frac{v^2}{c^2} = 1 \Rightarrow 1 - \beta^2 = 0$
 $\Rightarrow v'^2 = c^2 \left[1 - \frac{(1 - \beta^2)(1 - \beta_0^2)}{\left(1 - \frac{v_x v_0}{c^2} \right)^2} \right] = c^2 \rightarrow v' = c_0$

ABSOLUTNI ČAS

$$c \Delta t' = \gamma_0 (c \Delta t - \beta_0 \Delta x) \Rightarrow \Delta t' = \gamma_0 \left(\Delta t - \frac{\beta_0 \Delta x}{c} \right) \Rightarrow \text{v splošnem } \Delta t' \neq \Delta t$$

Primer: μ^\pm
 mion \rightarrow

S: mirovni sistem μ^\pm
 $t_1 = 0$ $t_2 = \tau \approx 2 \cdot 10^{-6} \text{ s}$ $c\tau \approx 600 \text{ m}$
 $x_1 = 0$ $x_2 = 0$
 $y_1 = 0$ $y_2 = 0$
 $z_1 = 0$ $z_2 = 0$

$$\rightarrow \Delta t = t_2 - t_1 = \tau$$

$$\gamma_0 = \frac{1}{\sqrt{1 - \beta^2}} > 1$$

S': $\vec{v}_0 = v_0 \hat{e}_x$ glede na S

$$t_1' = \gamma_0 \left(t_1 - \frac{\beta_0}{c} x_1 \right) = 0 \quad t_2' = \gamma_0 \left(t_2 - \frac{\beta_0}{c} x_2 \right) = \gamma_0 t_2$$

$$\rightarrow \Delta t' = t_2' - t_1' = t_2' = \gamma_0 \tau$$

LT $\Rightarrow \Delta t' > \Delta t$ (relativistično podaljšanje časa)
 $\Delta x \approx c_0 \Delta t$ ($\Delta t = \Delta t'$)
 Δt

c_0 in KAVZALNOST:

S: t_1 t_2 $t_2 > t_1 \Rightarrow \Delta t = t_2 - t_1 > 0$
 x_1 x_2
 $y_1 = 0$ $y_2 = 0$
 $z_1 = 0$ $z_2 = 0$

$$S': \left. \begin{aligned} t_1' &= \gamma_0 (t_1 - \frac{\beta_0}{c} x_1) \\ t_2' &= \gamma_0 (t_2 - \frac{\beta_0}{c} x_2) \end{aligned} \right\} \Rightarrow \Delta t' = t_2' - t_1' = \gamma_0 \left[\frac{t_2 - t_1}{\Delta t} - \frac{\beta_0 \Delta x}{c} \right]; \Delta x = x_2 - x_1$$

$$\Delta t' < 0; \text{ \u010e } \Delta t - \beta_0 \frac{\Delta x}{c} < 0 \rightarrow \Delta t < \frac{\beta_0 \Delta x}{c}$$

t_1 : A ustrelil; v
 $t_2 = t_1 + \Delta t$: zadane B $\Delta t = \frac{\Delta x}{v}$
 $\Delta t < 0 \Rightarrow \Delta t < \frac{\beta_0 \Delta x}{c} \rightarrow \frac{\Delta x}{v} < \frac{\beta_0 \Delta x}{c} \Rightarrow v > \frac{1}{\beta_0} c > c$ $\beta_0 < 1$
 \leftarrow kr\u0161itev kausalnosti
 C: $t_2' (< t_1')$ vidi: B pade

ABSOLUTNA RAZDALJA

S: $x_1 = 0$ ob (vsakem) \u010dasu t_1
 $x_2 = l$ ob (vsakem) \u010dasu t_2 ; l ... dol\u017einna rakete v sistemu S
 $D = |\vec{r}_1(t_1) - \vec{r}_2(t_2 = t_1)| = |x_1(t_1) - x_2(t_2 = t_1)| = l$

S': $D' = |\vec{r}_1'(t_1') - \vec{r}_2'(t_2' = t_1')|$
 $c t_1' = \gamma_0 (c t_1 - \beta_0 x_1) = \gamma_0 c t_1$
 $x_1' = \gamma_0 (x_1 - \beta_0 c t_1) = -\gamma_0 v_0 t_1$
 $y_1' = y_1$
 $z_1' = z_1$
 $c t_2' = \gamma_0 (c t_2 - \beta_0 l)$
 $x_2' = \gamma_0 (l - v_0 t_2)$
 $y_2' = y_2$
 $z_2' = z_2$
 $\rightarrow D' = |x_1'(t_1') - x_2'(t_2' = t_1')|$ $t_2' = t_1'$... razdalija med koncema rakete ob istem \u010dasu

$$c t_2' = c t_1'$$

$$\gamma_0 (c t_2 - \beta_0 l) = \gamma_0 (c t_1)$$

$$c t_1 = c t_2 - \beta_0 l \rightarrow t_2 = t_1 + \frac{\beta_0}{c} l$$

$$x_1'(t_1) = -\gamma_0 v_0 t_1$$

$$x_2'(t_2' = t_1') = \gamma_0 (l - v_0 t_2) = \gamma_0 (l - v_0 (t_1 + \frac{\beta_0}{c} l)) = \gamma_0 l (1 - \beta_0^2) - \gamma_0 v_0 t_1 = \frac{l}{\gamma_0^2} + x_1'(t_1)$$

$$\Rightarrow D' = |x_1'(t_1) - \frac{l}{\gamma_0} - x_1'(t_1)| = \frac{l}{\gamma_0}; \gamma_0 > 1 \Rightarrow D' < D$$

SKALARJI V PTR

Definicija: skalar \equiv invariantna na LT

\vec{r} ... kraj\u0161evni vektor T

$$r = \sqrt{\vec{r} \cdot \vec{r}} = \sqrt{\langle \vec{r}, \vec{r} \rangle}$$

$$O: O^T = O^{-1}$$

$$\vec{r}' = O \vec{r} \Rightarrow r'^2 = \langle \vec{r}', \vec{r}' \rangle = \langle O \vec{r}, O \vec{r} \rangle = \langle \vec{r}, O^T O \vec{r} \rangle = \langle \vec{r}, \vec{r} \rangle = r^2$$

$$r^2 = \langle \vec{r}, \vec{r} \rangle = \langle \mathbb{1}_{3 \times 3} \vec{r}, \vec{r} \rangle; \mathbb{1}_{3 \times 3} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}; \text{ evklidski prostor}$$

$$\Lambda = \begin{bmatrix} \gamma_0 & -\beta_0 \gamma_0 & 0 & 0 \\ -\beta_0 \gamma_0 & \gamma_0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad \Lambda^T \neq \Lambda^{-1} = \begin{bmatrix} \gamma_0 & \beta_0 \gamma_0 & 0 & 0 \\ \beta_0 \gamma_0 & \gamma_0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^4 X' = \Lambda {}^4 X$$

$${}^4 X'^2 = \langle \mathbb{1}_{4 \times 4} {}^4 X', {}^4 X' \rangle = \langle \Lambda {}^4 X, \Lambda {}^4 X \rangle = \langle {}^4 X, \Lambda^T \Lambda {}^4 X \rangle \neq \langle \mathbb{1}_{4 \times 4} {}^4 X, {}^4 X \rangle = {}^4 X^2$$

$$\Lambda \eta \Lambda = \eta \Rightarrow \eta \Lambda = \Lambda^{-1} \eta$$

$$\mathbb{1}_{4 \times 4} \rightarrow \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & -1 \end{bmatrix} = \eta$$

$$\langle \eta^{\mu} X^{\nu}, \eta^{\mu} X^{\nu} \rangle = \langle \eta^{\mu} \Lambda^{\mu} X^{\nu}, \eta^{\mu} X^{\nu} \rangle = \langle \Lambda^{\mu} \eta^{\mu} \Lambda^{\mu} X^{\nu}, \eta^{\mu} X^{\nu} \rangle = \langle \eta^{\mu} X^{\nu}, \eta^{\mu} X^{\nu} \rangle$$

$$\eta^{\mu} X^{\nu} = \eta^{\mu} [c \mathbf{t} \times \mathbf{y} \mathbf{z}]^T = \begin{bmatrix} c \mathbf{t} \\ -\mathbf{r} \end{bmatrix} = {}_4 X$$

$$\rightarrow \langle {}_4 X, {}_4 X \rangle = {}_4 X \cdot {}_4 X \quad \rightarrow \quad {}_4 X \cdot {}_4 X = {}_4 X' \cdot {}_4 X'$$

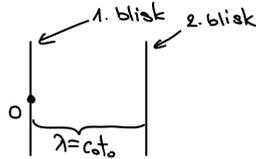
DOPLERJEV POŠAV

- mehansko valovanje: v glede na snov \leftarrow ne deluje
- elektro-magnetno valovanje v praznem prostoru: relativna hitrost

S: mirovni sistem oddajnika

1. blisk: $t_1 = t, x_1 = 0$

2. blisk: $t_2 = t_1 + t_0; x_2 = 0$



S': mirovni sistem sprejemnika, ki se giblje s hitrostjo $\vec{v}_0 = v_0 \hat{e}_x$ glede na S

$$\begin{aligned} t_1' &= \gamma_0 \left(t_1 - \frac{v_0}{c^2} x_1 \right) = \gamma_0 t_1 \\ x_1'(t_1) &= \gamma_0 (x_1 - v_0 t_1) = -\gamma_0 v_0 t_1 = -v_0 t_1' = x_1'(t_1) \\ t_2' &= \gamma_0 \left(t_2 - \frac{v_0}{c^2} x_2 \right) = \gamma_0 t_2 = \gamma_0 (t_1 + t_0) = \gamma_0 t_1 + \gamma_0 t_0 = t_1' + \gamma_0 t_0 \\ x_2'(t_2) &= \gamma_0 (x_2 - v_0 t_2) = -\gamma_0 v_0 t_2 = -v_0 t_2' = x_2'(t_2) \end{aligned}$$

tudi v S' se bliska gibljeta s c_0

$$x_1'(t_2) = x_1'(t_1) + c_0 (t_2' - t_1') = -v_0 t_1' + c_0 \gamma_0 t_0$$

$$\Delta l' = |x_1'(t_2) - x_2'(t_2)| = |-v_0 t_1' + c_0 \gamma_0 t_0 + v_0 t_2'| = |-v_0 t_1' + c_0 \gamma_0 t_0 + v_0 (t_1' + \gamma_0 t_0)| = |\gamma_0 t_0 (c_0 + v_0)| = \frac{(c_0 + v_0) t_0}{\sqrt{1 - \frac{v_0^2}{c_0^2}}} =$$

$$= \frac{(c_0 + v_0) c_0 t_0}{\sqrt{c_0^2 - v_0^2}} = \lambda \sqrt{\frac{c_0 + v_0}{c_0 - v_0}}$$

$$\left(\lambda' = \frac{c_0}{\lambda} = \sqrt{\frac{c_0 \mp v_0}{c_0 \mp v_0}} \frac{c_0}{\lambda} = \sqrt{\frac{c_0 \mp v_0}{c_0 \pm v_0}} \right)$$

ČETVEREC HITROSTI

Spomnimo se: $v^2 = c_0^2 \left[1 - \frac{(1 - \beta^2)(1 - \beta^2)}{\left(1 - \frac{v_0 v_x}{c_0^2}\right)^2} \right]; \beta^2 = \frac{v^2}{c_0^2}; \beta_0^2 = \frac{v_0^2}{c_0^2}$

$$\Rightarrow \frac{v^2}{c_0^2} = 1 - \frac{(1 - \beta^2)(1 - \beta^2)}{\left(1 - \frac{v_0 v_x}{c_0^2}\right)^2} \rightarrow 1 - \beta^2 = \frac{(1 - \beta^2)(1 - \beta^2)}{\left(1 - \frac{v_0 v_x}{c_0^2}\right)^2}$$

$$\rightarrow \frac{1}{\beta'^2} = \frac{1}{\beta_0^2 \beta^2 \left(1 - \frac{v_0 v_x}{c_0^2}\right)^2}; \beta_0^2 = \frac{1}{1 - \beta^2}; \beta'^2 = \frac{1}{1 - \beta^2}; \beta^2 = \frac{1}{1 - \beta^2}$$

$$\Rightarrow \frac{\beta_0'}{\beta_0} = \frac{1}{\beta_0} \frac{1}{1 - \frac{v_0 v_x}{c_0^2}} = \frac{dt}{dt'} \quad (= 1 / \frac{dt'}{dt})$$

4D-hitrost: ${}^4 u_{\mu} = \gamma \frac{d({}^4 X)}{dt}$

$${}^4 u' = \Lambda {}^4 u = \begin{bmatrix} \gamma c_0 \\ \gamma \vec{v} \end{bmatrix}$$

Dokaz: ${}^4 X' = \Lambda {}^4 X; \Lambda \neq \Lambda(t, x) \quad \frac{\partial \Lambda}{\partial t} + \frac{\partial \Lambda}{\partial x} \frac{dx}{dt} = 0$

$$\frac{d({}^4 X')}{dt} = \frac{d}{dt} (\Lambda {}^4 X) = \Lambda \frac{d({}^4 X)}{dt} + \left(\frac{d}{dt} \Lambda \right) \cdot {}^4 X = \Lambda \frac{d({}^4 X)}{dt}$$

$$\frac{d({}^4 X')}{dt'} = \frac{d({}^4 X)}{dt} \frac{dt}{dt'} = \Lambda \frac{d({}^4 X)}{dt} \frac{dt}{dt'} = \frac{1}{\beta'} \Lambda \frac{d({}^4 X)}{dt}$$

$$\Rightarrow \frac{\beta_0'}{\beta_0} \frac{d({}^4 X')}{dt'} = \frac{\Lambda \frac{d({}^4 X)}{dt}}{\Lambda {}^4 u} \quad \square$$

ČETVEREC POSPEŠKA

$$\left. \begin{matrix} {}^4u \\ \frac{d}{dt} \\ \times \gamma \end{matrix} \right\} \Rightarrow {}^4b = \gamma \frac{d}{dt} ({}^4u)$$

$$\frac{d}{dt} \gamma = \frac{d}{dt} \frac{1}{\sqrt{1-\frac{v^2}{c^2}}} = \frac{d}{dt} (1 - \frac{\vec{v}\vec{v}}{c^2})^{-\frac{1}{2}} = \frac{1}{2} (1 - \frac{\vec{v}\vec{v}}{c^2})^{-\frac{3}{2}} \cdot \frac{2\vec{v}\vec{a}}{c^2} = \gamma^3 \frac{\vec{v}\vec{a}}{c^2}$$

$${}^4b = \begin{bmatrix} \gamma^4 \frac{\vec{v}\vec{a}}{c^2} \\ \gamma^4 \frac{\vec{v}\vec{v}}{c^2} \vec{v} + \gamma^2 \vec{a} \end{bmatrix}$$

ČETVERCI 'P, 'F, 'j_e

$${}^4P = m_0 {}^4u = \begin{bmatrix} m_0 \gamma c_0 \\ m_0 \gamma \vec{v} \end{bmatrix} \leftarrow \text{ČETVEREC GIBALNE KOLIČINE}$$

↑ masa v mirovnem sistemu

$${}^4F = m_0 {}^4b = \begin{bmatrix} m_0 \gamma^4 \frac{\vec{v}\vec{a}}{c^2} \\ m_0 \gamma^4 \frac{\vec{v}\vec{v}}{c^2} \vec{v} + \gamma^2 \vec{a} \end{bmatrix} \leftarrow \text{ČETVEREC SILE}$$

$${}^4j_e = j_e {}^4u = \begin{bmatrix} j_e \gamma c_0 \\ j_e \gamma \vec{v} \end{bmatrix} \leftarrow \text{ČETVEREC GOSTOTE ELEKTRIČNEGA TOKA}$$

$${}^4P: m_0 \gamma c_0 = \frac{1}{c} (m c_0^2 \gamma) = \frac{E}{c} \Rightarrow \boxed{E = m c_0^2 \gamma}$$

$$= \frac{1}{c} (m c_0^2 \sqrt{1-\beta^2})$$

$$\beta \ll 1: \frac{1}{\sqrt{1-\beta^2}} \approx \frac{1}{1-\frac{1}{2}\beta^2} \approx 1 + \frac{1}{2}\beta^2$$

$$m_0 \gamma c_0 \approx \frac{1}{c} (m_0 c_0^2 (1 + \frac{1}{2}\beta^2)) = \frac{1}{c} (m_0 c_0^2 + \frac{1}{2} m_0 v^2)$$

$\frac{E_0}{c}$ $\frac{W_k}{c} (=T)$

$${}^4P = \begin{bmatrix} \frac{E}{c} \\ \vec{p} \end{bmatrix}$$

$$\vec{p} = m_0 \gamma \vec{v} \quad (v \ll c; \gamma \approx 1 \Rightarrow \vec{p} \approx m\vec{v})$$

$$\vec{p}\vec{p} = m_0^2 \gamma^2 v^2 \Rightarrow p^2 c^2 = m_0^2 \gamma^4 c^2 v^2 = m_0^2 c_0^4 v^2 \beta^2$$

$$E^2 - p^2 c^2 = m_0^2 c_0^4 \gamma^2 (1 - \beta^2) = m_0^2 c_0^4 \rightarrow \boxed{E^2 = p^2 c^2 + m_0^2 c_0^4}$$

$${}^4P \cdot {}^4P = \left[\frac{E}{c} \quad -\vec{p} \right]^T \cdot \left[\frac{E}{c} \quad \vec{p} \right]^T = \frac{E^2}{c^2} - p^2 = \frac{1}{c^2} (E^2 - p^2 c^2) = \frac{1}{c^2} m_0^2 c_0^4 = m_0^2 c_0^2$$

$$E = m \gamma c_0^2 = m c_0^2 \frac{1}{\sqrt{1-\beta^2}} \quad v \rightarrow c_0 \Rightarrow \beta \rightarrow 1 \Rightarrow \gamma \rightarrow \infty \Rightarrow E \rightarrow \infty$$

Primer: (LEP)

↑ elektron-volt

$$e^\pm; m_0 c^2 \approx 0,5 \text{ MeV} = 0,5 \cdot 10^6 \cdot 1,6 \cdot 10^{-19} \text{ J}$$

$$E = 100 \text{ GeV} = 100 \cdot 10^9 \cdot 1,6 \cdot 10^{-19} \text{ J}$$

$$\Rightarrow \frac{m c_0^2}{E} = \frac{1}{\gamma} = 0,5 \cdot 10^{-5}$$

$$\frac{1}{\gamma^2} = 0,25 \cdot 10^{-10} = 1 - \beta^2$$

$$\beta^2 = 1 - 0,25 \cdot 10^{-10} \Rightarrow \beta = 1 - 0,125 \cdot 10^{-10} \Rightarrow v = c_0 \beta$$

ČETVEREC LORENTZOVE SILE

$$\boxed{{}^4F' = \Lambda {}^4F} \quad ({}^4F' \neq {}^4F) \quad (\vec{F}' = \vec{F})$$

$$\vec{F} = q(\vec{E} + \vec{v}_q \times \vec{B})$$

$$M = \begin{bmatrix} 0 & -\frac{F_x}{c} & -\frac{F_y}{c} & -\frac{F_z}{c} \\ \frac{q\vec{v}_q \cdot \vec{E}}{c} & 0 & -B_z & B_y \\ \frac{q\vec{v}_q \cdot \vec{E}}{c} & B_z & 0 & -B_x \\ \frac{q\vec{v}_q \cdot \vec{E}}{c} & -B_y & B_x & 0 \end{bmatrix} \quad (6 \text{ neodvisnih elementov})$$

$${}^4u = \eta {}^4u = \begin{bmatrix} \gamma c \\ -\gamma \vec{v} \end{bmatrix}$$

$$\boxed{{}^4F_L = q M {}^4u} \leftarrow \text{ČETVEREC LORENTZOVE SILE}$$

$$= q \cdot \begin{bmatrix} \gamma \frac{\vec{E} \cdot \vec{v}}{c} \\ \gamma (\vec{E} + \vec{v} \times \vec{B}) \end{bmatrix} = \begin{bmatrix} F_{L0} \\ \vec{F}_L \end{bmatrix}$$

$$\vec{F}_L = \gamma q (\vec{E} + \vec{v} \times \vec{B}); \quad |\vec{v}| \ll c \Rightarrow \beta \ll 1 \Rightarrow \gamma \approx 1 + \frac{\beta^2}{2} = 1 + O(\beta^2)$$

$$\vec{v} \times \vec{B} = -\vec{B} \times \vec{v} = \vec{B} \times (-\vec{v}) = \begin{bmatrix} 0 & -B_z & B_y \\ B_z & 0 & -B_x \\ -B_y & B_x & 0 \end{bmatrix}$$

$$S \rightarrow S': \quad {}^4F' = \Lambda {}^4F \quad \Lambda \eta \Lambda = \eta \Rightarrow \eta \Lambda = \Lambda' \eta$$

$$q' = q$$

$${}^4u' = \eta' {}^4u' = \eta {}^4u = \eta \Lambda {}^4u = \Lambda^{-1} \eta {}^4u = \Lambda' {}^4u$$

$$\boxed{{}^4F'_L = q' M' {}^4u'} \quad \text{relativistični princip}$$

$$\Lambda' {}^4F_L = q M' \Lambda' {}^4u$$

$$\Lambda' \rightarrow \boxed{{}^4F_L = q \Lambda' M' \Lambda' {}^4u}$$

$$\Rightarrow \Lambda' M' \Lambda' = M$$

$$\Rightarrow \boxed{M' = \Lambda M \Lambda} \quad (M \text{ tenzor})$$

$$M' = \begin{bmatrix} 0 & -\frac{F'_x}{c} & -\frac{F'_y}{c} & -\frac{F'_z}{c} \\ \frac{q\vec{v}' \cdot \vec{E}'}{c} & 0 & -B'_z & B'_y \\ \frac{q\vec{v}' \cdot \vec{E}'}{c} & B'_z & 0 & -B'_x \\ \frac{q\vec{v}' \cdot \vec{E}'}{c} & -B'_y & B'_x & 0 \end{bmatrix} \quad \begin{aligned} \frac{F'_x}{c} &= \frac{F_x}{c} \\ \frac{F'_y}{c} &= \gamma_0 \left(\frac{F_y}{c} - \beta_0 B_z \right) \\ \frac{F'_z}{c} &= \gamma_0 \left(\frac{F_z}{c} + \beta_0 B_y \right) \end{aligned} \quad \begin{aligned} B'_x &= B_x \\ B'_y &= \gamma_0 (B_y + \beta_0 \frac{F_z}{c}) \\ B'_z &= \gamma_0 (B_z - \beta_0 \frac{F_y}{c}) \end{aligned}$$

$$\text{V vektorski obliki: } \frac{\vec{F}'}{c} = \gamma_0 (\frac{\vec{E}}{c} + \vec{\beta}_0 \times \vec{B}) - (\gamma_0 - 1) \hat{e}_x (\frac{\vec{E}}{c} \cdot \hat{e}_x); \quad \hat{e}_0 = \hat{e}_x \wedge \vec{\beta}_0 = \beta_0 \hat{e}_0 = \frac{v_0}{c} \hat{e}_x$$

$$= \frac{\vec{E}}{c} + \vec{\beta}_0 \times \vec{B} + (\gamma_0 - 1) \left[\frac{\vec{E}}{c} + \vec{\beta}_0 \times \vec{B} - \hat{e}_x (\frac{\vec{E}}{c} \cdot \hat{e}_x) \right]$$

$$\beta_0 \ll 1, \gamma_0 - 1 = O(\beta^2): \quad \approx \frac{\vec{E}}{c} + \vec{\beta}_0 \times \vec{B}$$

$$\vec{B}' = \gamma_0 (\vec{B} - \vec{\beta}_0 \times \frac{\vec{E}}{c}) - (\gamma_0 - 1) \hat{e}_x (\vec{B} \cdot \hat{e}_x)$$

$$= \vec{B} - \vec{\beta}_0 \times \frac{\vec{E}}{c} + (\gamma_0 - 1) [\vec{B} - \vec{\beta}_0 \times \frac{\vec{E}}{c} - \hat{e}_x (\vec{B} \cdot \hat{e}_x)]$$

$$\beta_0 \ll 1: \quad \approx \vec{B} - \vec{\beta}_0 \times \frac{\vec{E}}{c}$$

MAXWELLOVE ENAČBE in PTR

$$N = \begin{bmatrix} 0 & -\dot{b}_x & \dot{b}_y & \dot{b}_z \\ \dot{b}_x & 0 & \dot{b}_z & \dot{b}_y \\ \dot{b}_y & -\dot{b}_z & 0 & \dot{b}_x \\ \dot{b}_z & \dot{b}_y & -\dot{b}_x & 0 \end{bmatrix}$$

$$N' = \begin{bmatrix} 0 & -\dot{b}'_x & \dot{b}'_y & \dot{b}'_z \\ \dot{b}'_x & 0 & \dot{b}'_z & \dot{b}'_y \\ \dot{b}'_y & -\dot{b}'_z & 0 & \dot{b}'_x \\ \dot{b}'_z & \dot{b}'_y & -\dot{b}'_x & 0 \end{bmatrix} \quad N' = \Lambda N \Lambda \quad (N \text{ tenzor})$$

$$\begin{aligned} \rho &= \frac{1}{c_0} \frac{\partial \rho}{\partial t} \\ \rho_1 &= \frac{1}{c_0} \frac{\partial \rho}{\partial t} \\ \rho_2 &= \frac{1}{c_0} \frac{\partial \rho}{\partial t} \\ \rho_3 &= \frac{1}{c_0} \frac{\partial \rho}{\partial t} \end{aligned} \quad \rho' = \begin{bmatrix} \rho_0 \\ \rho_1 \\ \rho_2 \\ \rho_3 \end{bmatrix} = \begin{bmatrix} \frac{1}{c_0} \frac{\partial \rho}{\partial t} \\ \frac{1}{c_0} \frac{\partial \rho}{\partial t} \\ \frac{1}{c_0} \frac{\partial \rho}{\partial t} \\ \frac{1}{c_0} \frac{\partial \rho}{\partial t} \end{bmatrix}$$

$$\begin{aligned} \rho'_0 &= \Lambda^1 \rho_0 : \rho'_0 = \frac{1}{c_0} \frac{\partial \rho}{\partial t'} = \frac{1}{c_0} \left(\frac{\partial \rho}{\partial t} + \frac{\partial x}{\partial t} \frac{\partial \rho}{\partial x} \right); \quad t = \gamma_0 (t' + \frac{v_0}{c_0^2} x); \quad x = \gamma_0 (x + v_0 t) \\ &= \frac{v_0}{c_0} \left[\frac{\partial \rho}{\partial t} + v_0 \frac{\partial \rho}{\partial x} \right] \\ &= \gamma_0 [\rho_0 + \beta_0 \rho_1] \end{aligned} \quad \rho'_1 = \gamma_0 [\rho_1 + \beta_0 \rho_0]$$

$$\rho'_j = \gamma_0 \rho_j = \begin{bmatrix} \beta_0 \gamma_0 c_0 \\ \gamma_0 \gamma_j \end{bmatrix} = \begin{bmatrix} \rho_0 \\ \rho_j \end{bmatrix} = \begin{bmatrix} \rho_0 \\ \rho_j \end{bmatrix}; \quad \rho'_j = \rho_j$$

$$\rho'_j = [\rho_0 \quad \rho_1 \quad \rho_2 \quad \rho_3]$$

$$S: \begin{cases} (\rho'_j M)^T = \mu_0 \rho'_j \\ (\rho'_j N)^T = 0 \end{cases} \leftarrow \text{MAXWELLOVE ENAČBE}$$

$$(\rho'_j N)^T = \left(\begin{bmatrix} \frac{1}{c_0} \frac{\partial \rho}{\partial t} & \frac{\partial \rho}{\partial x} & \frac{\partial \rho}{\partial y} & \frac{\partial \rho}{\partial z} \end{bmatrix} \cdot N \right)^T = \begin{bmatrix} \vec{\nabla} \cdot \vec{B} \\ -\frac{1}{c_0} \frac{\partial B_x}{\partial t} - \frac{1}{c_0} \left(\frac{\partial F_x}{\partial y} - \frac{\partial F_y}{\partial x} \right) \\ -\frac{1}{c_0} \frac{\partial B_y}{\partial t} + \frac{1}{c_0} \left(\frac{\partial F_x}{\partial x} - \frac{\partial F_x}{\partial x} \right) \\ -\frac{1}{c_0} \frac{\partial B_z}{\partial t} - \frac{1}{c_0} \left(\frac{\partial F_x}{\partial x} - \frac{\partial F_x}{\partial x} \right) \end{bmatrix} = \begin{bmatrix} \vec{\nabla} \cdot \vec{B} \\ -\frac{1}{c_0} \left(\frac{\partial \vec{B}}{\partial t} + \vec{\nabla} \times \vec{E} \right) \end{bmatrix} = 0$$

$$\rightarrow \vec{\nabla} \times \vec{E} + \frac{\partial \vec{B}}{\partial t} = 0 \rightarrow \vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

(Podobno dobimo ostale Maxwellove enačbe.)

$$S': \begin{cases} (\rho'_j M')^T = (\rho'_j \Lambda^T \Lambda M \Lambda)^T = (\rho'_j M \Lambda)^T = \Lambda^T (\rho'_j M)^T = \Lambda \mu_0 \rho'_j = \mu_0 \Lambda^1 \rho'_j = \mu_0 \rho'_j \\ \rho'_j M' = (\Lambda^1 \rho'_j)^T = \rho'_j \Lambda^T = \rho'_j \Lambda^1 \end{cases}$$

ZAKLJUČEK

$$\rho'_j X = \begin{bmatrix} c_0 t \\ \vec{r} \end{bmatrix} \quad S \rightarrow S': \rho'_j X' = \Lambda^1 \rho'_j X$$

$$\rho'_j u = \gamma_0 \frac{d}{dt} (\rho'_j X) \quad \rho'_j b = \gamma_0 \frac{d}{dt} (\rho'_j u) \quad \rho'_j p = m_0 \rho'_j u \quad \rho'_j F = m_0 \rho'_j b \quad \rho'_j j = \rho_0 \rho'_j u$$

$$\rho'_j E = q M \rho'_j u$$

$$(\rho'_j N)^T = 0$$

$$(\rho'_j M)^T = \mu_0 \rho'_j j$$

$$\vec{E} = \zeta \vec{j}$$